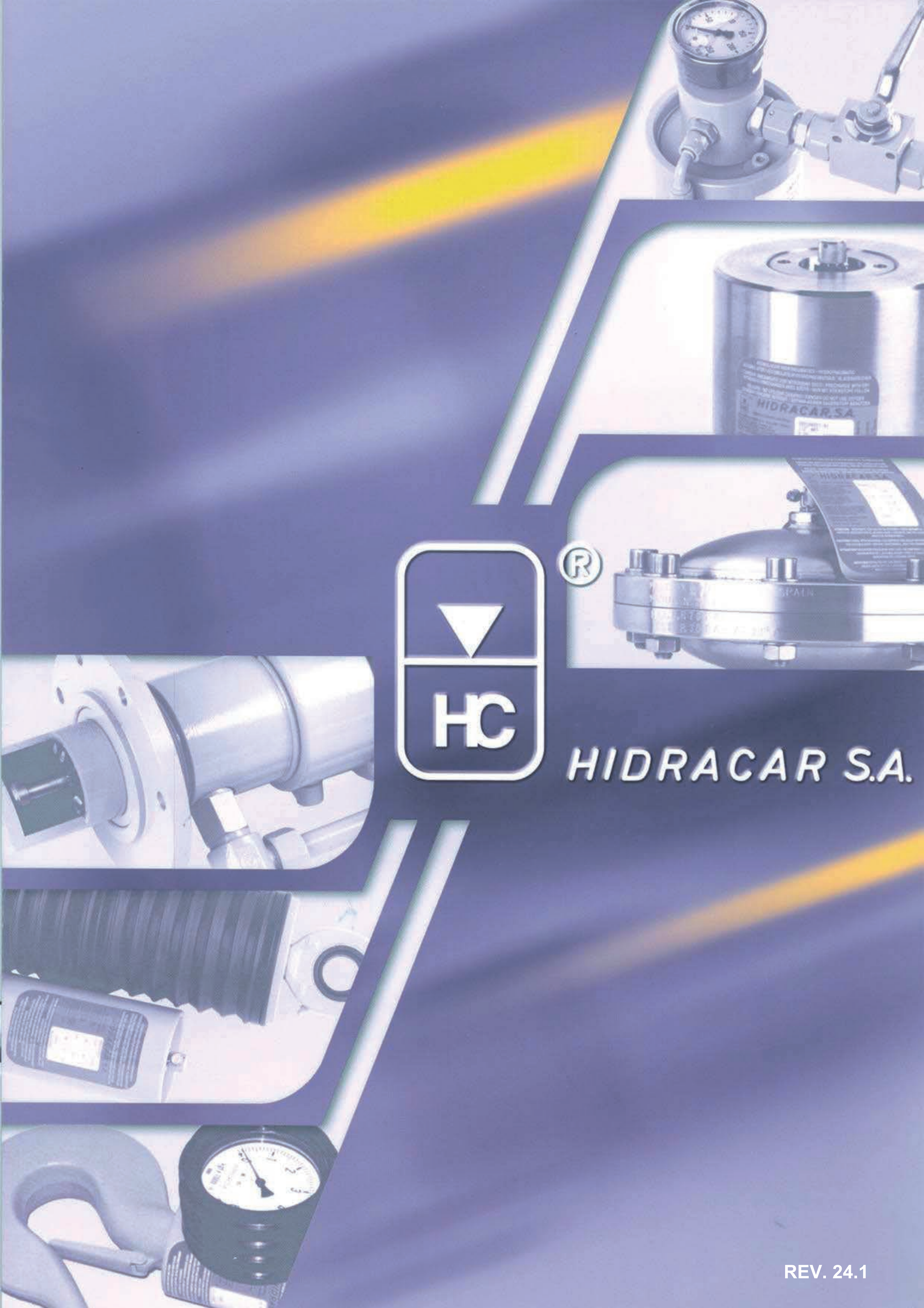

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EXPIRES: **October 12, 2024**

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HIDRACAR S.A.

SOME TECHNICAL AND PRACTICAL RECOMMENDATIONS ABOUT PULSATION DAMPENERS IN CIRCUITS WITH DOSING OR VOLUMETRIC PUMPS

DESCRIPTION OF A PULSATION DAMPENER AND HOW IT WORKS

A pulsation dampener is a vessel with pressurized gas inside, normally **nitrogen**. The initial filling or inflating gas pressure inside the dampener must always be lower than the pressure of the circuit where it is installed. The inflating gas pressure of the dampener will be called “$\mathbf{P_0}$”.

In all pulsation dampeners there is a separator element to isolate the gas from the circuit liquid; its main function being to avoid gas leaks. This part that separates both fluids is made basically in two kinds of material: Rubber (**NBR, EPDM, FKM, butyl, silicone,** etc,...) or a thermoplastic material, usually **PTFE**. When rubber is used, the separator element is called bladder and if the **PTFE** is used the dampener can be either membrane or bellows type according to the form of the separator element. The bellows can also be made in stainless steel. The use of one type of separator or another will generally depend on the particular characteristics of the circuit, such as: the working pressure, temperature and the possible corrosive effect of the circuit liquid over the separator element. Below in **Figure 1,** are shown the ***HIDRACAR S.A.*** three different dampeners type mentioned before.

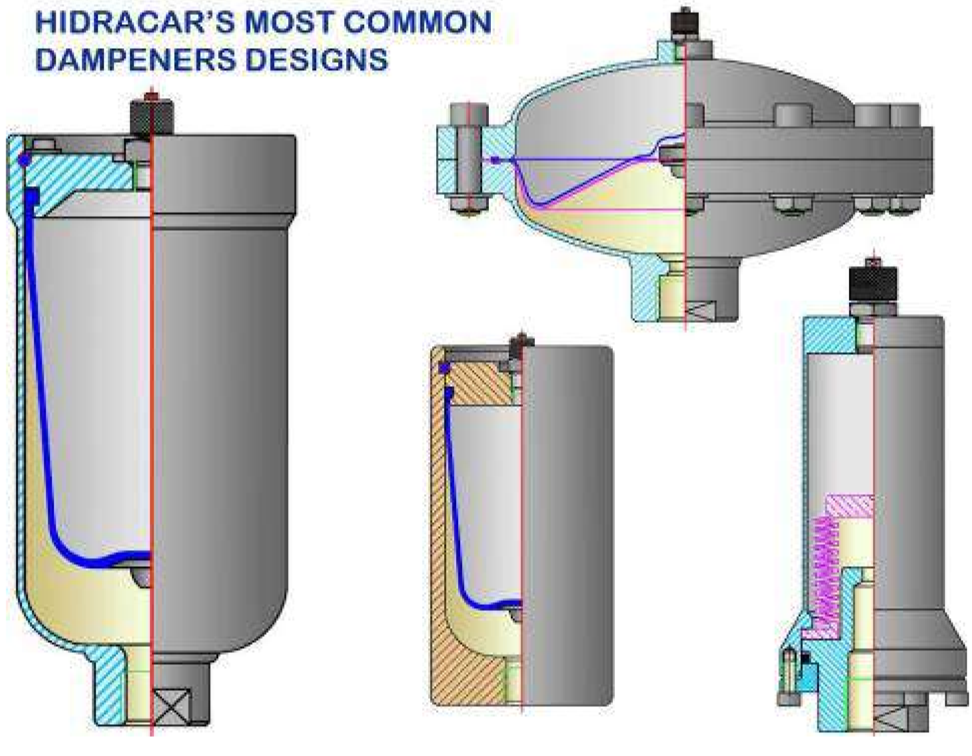


Figure 1. HIDRACAR’s cost common dampeners designs. (Bladder, Bellows and membrane types)

THE FUNCTION of a pulsation dampener is to stabilize the variable and oscillating flow generated in a hydraulic circuit in each cycle by volumetric piston or membrane pumps such as dosing or metering pumps. The main function of these pumps being to deliver a constant volume of liquid in every cycle independently of the circuit resistance or pressure (we will later see the characteristics of this kind of pumps), and that’s why a pulsation dampener ought to be installed.

When there is a pulsation dampener installed in the circuit, the volume supplied by the pump in every impulse or work cycle is divided in two parts; one goes to the circuit and the other part goes into the pulsation dampener. This volume stored into the dampener is returned right after back into the circuit while the pump is in its suction or chamber filling stage. The amount of liquid going in and out of the dampener in each alternating cycle of the pump will be called “**δV**”.

When δV gets introduced into the dampener the gas contained inside will be compressed and, therefore, its volume reduced and the pressure increased. The final gas volume (V_2) will be the initial gas volume minus the volume of liquid introduced (δV).

The initial gas volume is the total volume of the dampener or the size of the dampener. The size of the dampener is an unknown value to be calculated in every case depending on the kind of pump. This volume or size of the dampener will be called "V_0"

From all this, we can establish that: $$V_2 + \delta V = V_0$$

Every dampener has a constant derived from its size and its filling or charging gas pressure (Boyle-Mariotte law)**:**

$$P_0 \times V_0 = \text{constant } (*)$$

(*) This law is only applicable for ideal gases. In practice, this law is not accomplished; later on we will come back to this matter.

In working practice, it is not convenient for the dampeners to get totally emptied of the liquid in each cycle. An extra volume "**v**" is recommended to avoid the anti-extrusion insert of the separator element from repeatedly hammering against the internal bottom surface of the dampener, what could wear prematurely the bladder or membrane out. A new formula results from it:

$$V_2 + \delta V + v = V_0$$

where "**v**" is a theoretical unused volume of liquid inside the dampener, it is the volume of liquid permanently stored in the dampener. As a norm this volume is considered to be **20%** of the total dampener volume, as long as the temperature remains constant, and, therefore the former formula can be expressed as:

$$V_2 + \delta V + 0.2\, V_0 = V_0 \qquad \text{and finally as:} \qquad V_0 = (V_2 + \delta V) / 0.8$$

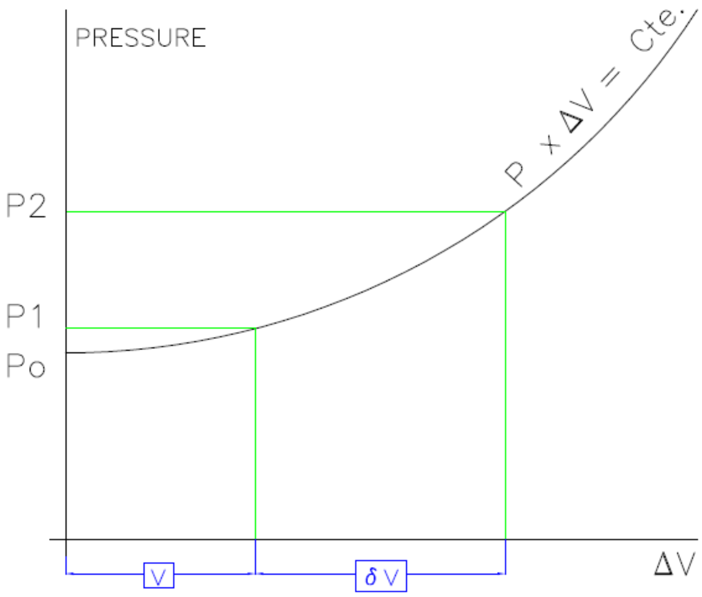


Figure 2. Graph of internal pressure in a dampeners against the volume fluctuations.

The graph in **Figure 2** represents the curve (hyperbola) of gas compression inside the accumulator or pulsation dampener. It is represented the pressure of the gas inside the accumulator against the volume fluctuations.

In the **Figure 3**, we can see the gas volume and pressure evolution at 3 stages (pre-charge, P1 and P2 which are the minimum and maximum pressures in the circuit once the pump is functioning).

At the initial gas charge pressure value "P_0" there is no liquid inside the dampener and the gas fills the whole dampener interior. The curve cuts the ordinate axis in that point where the pressure value is "Po". In the abscissa axis is represented the volume of liquid introduced into the dampener in each working cycle.

The pressure "P_1" is the gas pressure when a volume "**v**" has been introduced into the dampener. The pressure "P_2" is the value reached by the gas when the additional volume "**δV**" is introduced into the dampener.

From the curve in **Figure 2** we can deduce that for a fixed dampener size if the value "**δV**" increases then the pressure value "P_2" will also increase; or the other way around: If we increase the dampener size keeping constant the value "**δV**" the final pressure gas value "P_2" will be lower.

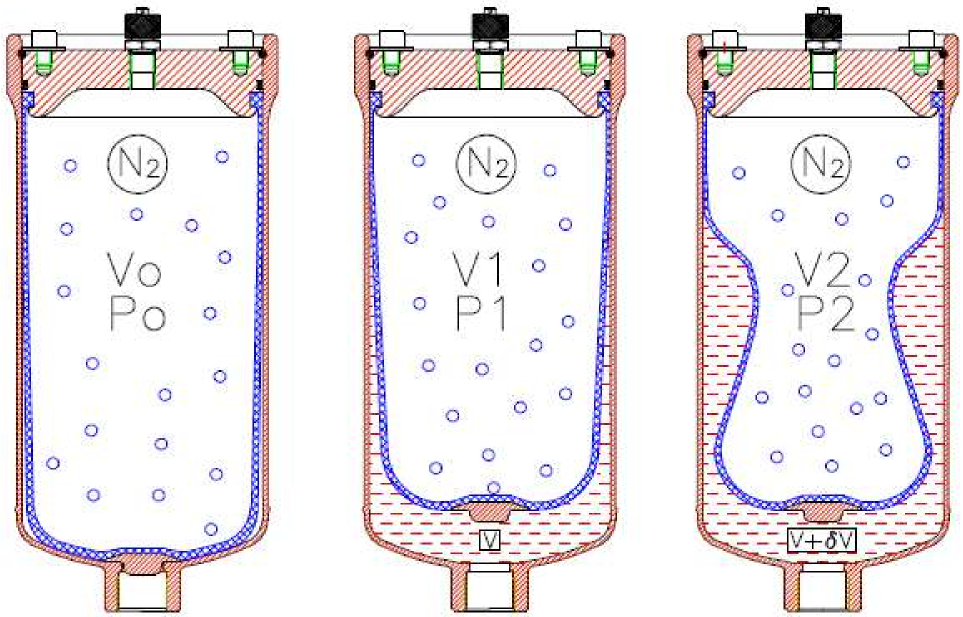


Figure 3. Bladder type dampener in its three stages or internal gas volumes

DAMPENER SIZE CALCULATION

The data needed to calculate the dampener size are:

"**δV**" = Volume of liquid that the dampener must store (in the chapter describing the different types of dosing pumps we will see the relation between "**δV**" and the cubic capacity of each of the three most common types of pumps).

"P_1" and "P_2" are the minimum and maximum pressure values that are accepted in the circuit.

Note: A pulsation dampener does not eliminate 100% of the pressure oscillation produced in the circuits with volumetric or dosing pumps. Its function is to regulate or control the variations of pressure so it remains within previously set limits. This variation, as a +/- percentage of the theoretical pressure "P_t", *is what determines, together with the value of* "**δV**", the size of the pulsation dampener.

"P_t" is the pressure needed at the pump outlet, in order to overcome all the resistances that will arise, to circulate the liquid all the way to the end of the hydraulic circuit.

Let's see an example: If the theoretical or work pressure in a circuit is "P_t" and the residual pulsation admitted is **+/- 5%** of this pressure, values P_1 and P_2 will be:

$$P_1 = P_t - (5/100) \times P_t \quad \text{and} \quad P_2 = P_t + (5/100) \times P_t$$

With all this known data: **δV**, **P_1** and **P_2**, we can already calculate the dampener size "**V_0**".

The ideal gas law in isothermal conditions (Boyle's law) (later on we will clarify this equation for this application) gives us the following equality:

$$P_0 \times V_0 = P_1 \times V_1 = P_2 \times V_2 = \text{Constant}. \quad (1)$$

If: $V_1 = V_0 - v$ and $v = 0.2 \times V_0$

we have: $V_1 = 0.8 \times V_0$ (2)

and also: $V_2 = V_1 - \delta V$ (3)

Finally, from (1) and (2) we obtain: $P_0 = 0.8 \times P_1$ (4)

and then from (1), (2), (3) and (4) we will get:

$$P_0 \times V_0 = P_2 \times V_2 ; \quad 0.8\, P_1 \times V_0 = P_2 \times (V_1 - \delta V) = P_2\,(0.8\, V_0 - \delta V)$$

From the underlined ends of the equalities we obtain the final formula:

$$V_0 = \frac{P_2 \times \delta V}{0.8\,(P_2 - P_1)} \quad (5)$$

This is the simplified theoretical formula to calculate the pulsation dampener volume as a function of **δV**, **P_1** and **P_2**.

As we have already said, it is accepted as a norm that the charging gas pressure, "**P_0**" **= 0.8 P_1**. This difference between **P_0** and **P_1** prevents the complete emptying of liquid from the dampener in each work cycle. Having this extra quantity of liquid **"v"** (stored in the dampener in between **P_0** and **P_1**) can also be used to compensate, in some instances, the potential changes in the gas pressure produced by variations in the exterior temperature that would modify the calculated theoretical "**δV**" and in that case it could not be completely introduced into or discharged out of the dampener.

The former equality (1) **$P_0 \times V_0 = P_1 \times V_1 = ... = P_n \times V_n$** does not comply in practice because, when a volume of gas is compressed (in a short time), the temperature rises, what increases the pressure, and when a gas expands its pressure drops an extra value because the temperature is reduced (refrigerator effect). This effect happens with the majority of gases, included Nitrogen and air, which are the more commonly used for charging the dampeners (atmospheric air can be used for pressures below **10 bar**, providing there is no risk of chemical reaction between the Oxygen in the air and the pumped liquid).

The formula (1) gets, thus, transformed into:

$$P_0 \times V_0^{\gamma} = P_1 \times V_1^{\gamma} = ... = P_n \times V_n^{\gamma} \quad (6)$$

where **γ** = specific heat ratio of the gas at constant pressure and volume, respectively. For ideal diatomic gases (N_2), **$\gamma = 1.4$** This constant is also theoretical.

We can obtain from both formulas (5) and (6), the **Vo** as a function of the residual pulsation.

If we consider **Θ= ± residual pulsation (%) / 100**

From (5). Isotherm curve

$$V_0 = \frac{1 + \Theta}{1{,}6\Theta}\, \delta V \quad (5.1)$$

From (6). Adiabatic curve

$$Vo = \frac{1}{\left(\frac{0.8}{1-\theta}\right)^{1/\gamma} - \left(\frac{0.8}{1+\theta}\right)^{1/\gamma}}\, \partial V \quad (6.1)$$

If we divide the above formulas (5.1 for Isotherm curve) divided by (6.1 for Adiabatic curve), we obtain a relation **K** which is function of the residual pulsation **ϴ**. For low values of admissible residual pulsations (below +-5%), the value obtained is practically constant (**K=0,8).** So, we will incorporate the factor **K** in the formula (5), to take in consideration the adiabatic expansion and compression of the gas inside the dampener:

$$\mathbf{V_0 = \frac{P_2 \times \delta V}{0.8 \times 0.8 \times (P_2 - P_1)}} \qquad (7)$$

This formula can be used in practice for nearly all industrial applications. It will be very unlikely for the volumes given by this formula to fit any standard dampener volume size from a manufacturer. Except for very exigent applications we can recommend to use the manufacturer's standard closer lower size, favouring cost efficiency.

Note: We have not considered a possible temperature variation of the fluid or environment. This would change the charging gas pressure value at 20º (take note that for each 10ºC variation in temperature the gas pressure will change approximately by 3%).

DIFFERENT TYPES OF DOSING PUMPS TO WHICH A DAMPENER CAN BE MOUNTED

We will consider pumps with one, two or three pistons and crankshaft movement being these the most extended and used and also those in bigger need for a dampener (for air operated, peristaltic, etc... pumps please consult ***HIDRACAR S.A.*** technical department).

The graphics below in **Figure 4** corresponds to these three types of piston pumps and represent the instantaneous flow during a complete crankshaft revolution. We have taken the same piston dimensions (diameter x stroke) for all three types of pumps.

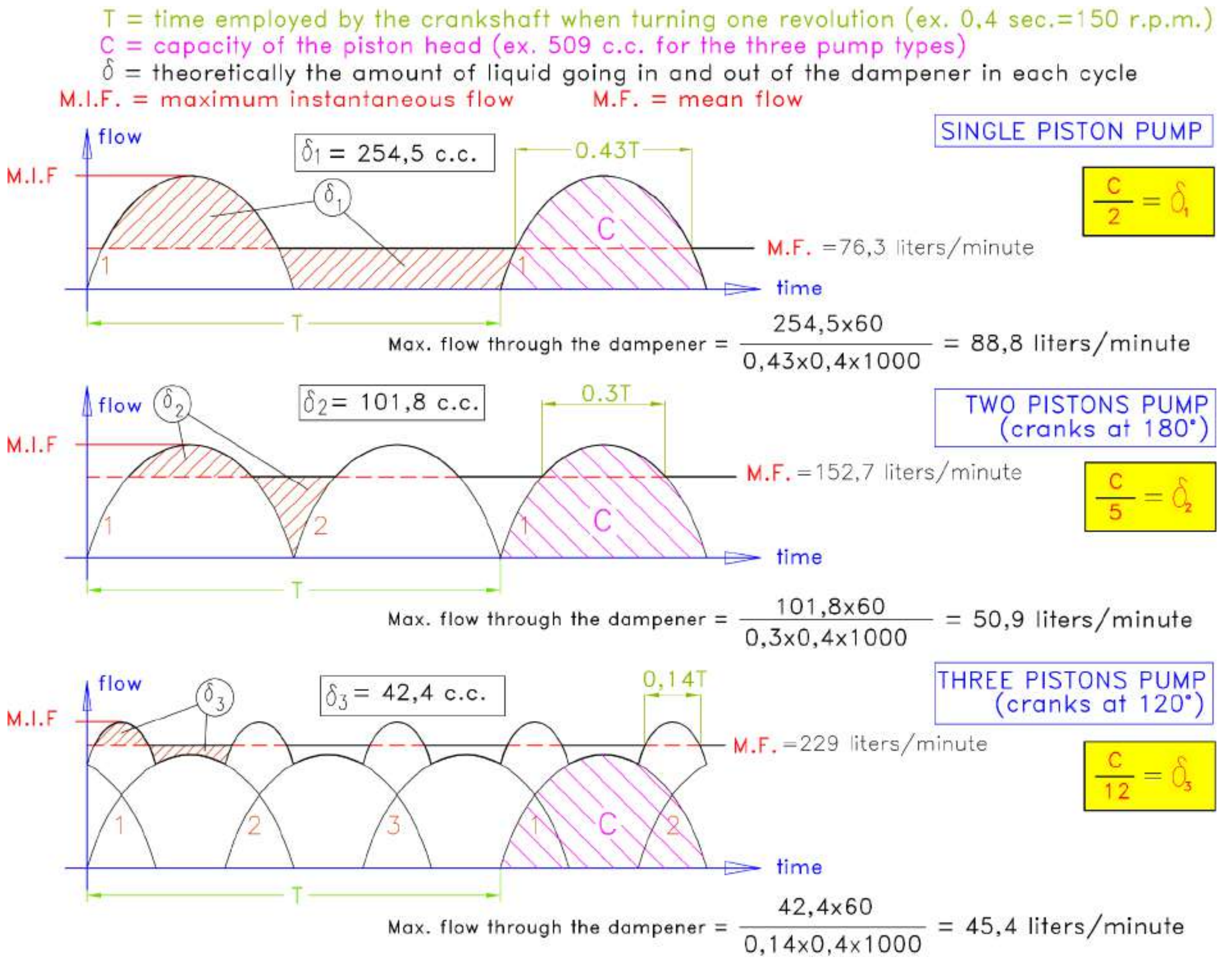


Figure 4. Graph for the instantaneous flow evolution in different pump types. From up to down: 1 piston pump, 2 piston pumps, 3 piston pumps (all of them single acting)

The curves in **Figure 4** let us see how a pulsation dampener works: If we pay attention to the first curve (on the top), representing a single piston pump, we can observe that for this type of pump the use of a dampener is almost essential, as otherwise during half revolution of the pump crankshaft no liquid flow is delivered. Also if the pump does not include a dampener, the diameter of the pipe must be calculated for the maximum instantaneous flow, which takes place when the piston speed is also at its maximum, in the middle of piston stroke (the flow curve is a sinusoid).

With a dampener installed in the pump outlet, the circuit flow will became practically constant. Hence, the pipe diameter downstream the dampener can be designed considering the mean flow. It makes possible to reduce the pipe diameter **by approximately 40%!!** And this because the maximum instantaneous flow of the pump is **2.8** times superior to its mean flow. In some cases this reduction of pipe diameter will compensate the cost of the dampener; furthermore the dampener will stabilize the circuit's pressure, with all of its obvious associated improvements (pressure in a hydraulic circuit is, basically, a function of the flow and losses of head).

Carrying on with the first curve in **Figure 4**, we can see that the task of the dampener is to store all the excess volume over the mean flow line. It occurs during the piston head impulse stroke; and then this volume "δ_1" is returned back into the circuit during the piston suction stroke. So then, in this type of pump the volume stored by the dampener is half of the pump head or capacity per revolution.

As we analyse all three curves in **Figure 4**, we can see that, as the number of pistons in a pump increase, the mean flow gets closer and closer to the maximum instantaneous flow and the liquid volume "δ_1" stored by the dampener gets correspondingly reduced, and therefore the required size of the dampener also gets reduced (this is totally valid in a case like this, where all the pistons in the three pumps have the same diameter, stroke and number of revolutions per minute).

The relation between "**δV**" and the capacity per head "**C**" is

$\delta v = C / 2$ For a one piston pump

$\delta v = C / 5$ For a two piston pump

$\delta v = C / 12$ For a three piston pump

(Practical values for the calculation of the dampener size).

We know that when a gas is compressed its pressure increases, and decreases if it expands its volume. When a dampener is installed in the outlet of a piston pump, the pressure of the liquid in the circuit will fluctuate according to the values of the volume of gas inside the dampener. This pressure variability (a +/- percentage of pressure P_t) will be defined by the technical designer of the circuit or by final customer requirements.

The following graphs in **Figure 5** will help to better understand the above exposed:

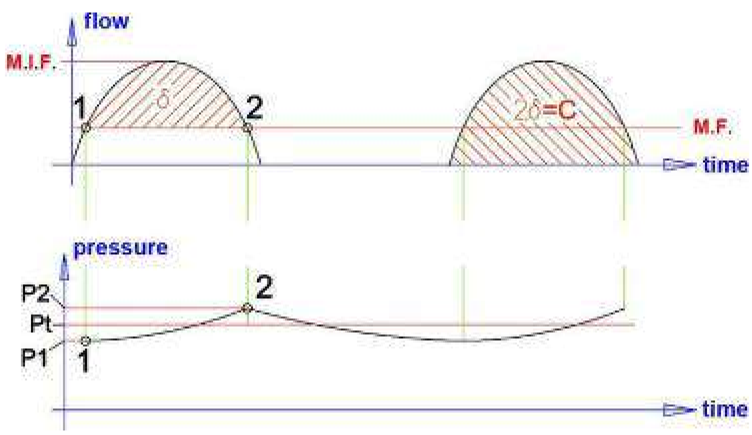


Figure 5. Pressure evolution in 1 piston pump complete cycle with the installation of a pulsation dampener.

Before all, let's consider that for the mean flow (M.F. in the graph) corresponds the working pressure "P_t". When the pump is in its impulsion cycle and the instantaneous flow increases and achieves the point 1 in the graph of the **Figure 5**, the dampener starts to store liquid (see in the top graph which represents the instantaneous flow delivered by the pump and the lower graph where the pressure variability with the use of a dampener is represented). The dampener ought to be charged at the adequate inflating pressure (80% of the working pressure). In the point **1** the damper starts to store liquid, in the point **2** the damper is full of liquid (all "**δV**" has been introduced in the damper). In the pump suction stroke, the damper discharges the volume "**δV**" previously stored.

The lower curve of the **Figure 5** shows the pressure fluctuation of a circuit with a dampener installed. This curve relates to the pump flow variation curve. As we have seen before, a dampener stores the volume of liquid above the pump mean flow. For this reason, the minimum value of the pressure curve (point **1**) must coincide with the first crossing point of the instantaneous flow curve with the line of the mean flow (the time where begins the liquid storage inside the dampener); and the maximum value of the pressure curve (point **2**) must coincide with the second crossing point between them (the time where finishes the liquid storage inside the dampener), in between these 2 points all the stored volume "**δV**" has been introduced inside the dampener.

Let's remember that the area comprised between the instantaneous flow curve and the abscissa axis (time) in Figure 5 top graph represents a volume which in the case of a single piston pump is equal to the pump capacity per stroke or revolution. (flow x time = volume) .

Let's see now the meaning of P_1, P_t and P_2 in the pressure / time curve of **Figure 5**:

In all hydraulic circuits the pressure at the pump outlet port is a function of the flow, pipe length and diameter, viscosity of the pumped liquid, internal pipe surface roughness, geometric height, etc... If the flow keeps constant over time, the pressure needed to pump the liquid will also be constant as long as there is no change either in flow resistance (for instance, due to sedimentation on filters, etc...) We call this constant working pressure or "P_t".

When designing a circuit, the mean flow and the opposing resistances shall be considered to calculate the pressure "P_t".

We have seen that the dampener stabilizes the flow and in fact also the pressure, the pressure in the circuit with a pulsation dampener installed varies from "P_1" to "P_2". The reason behind this is that the dampener has to stabilize the flow and for that it needs to compress and expand a volume of gas, and these pressure variations in +/- percentage of P_t are those that regulate the values accepted in the circuit.

We have already seen that this pressure fluctuation can be reduced to very small values by increasing the volume of the dampener. "P_1" and "P_2" are the minimum and maximum pressures in the circuit and can be expressed as a percentage value of "P_t". The end user or the circuit designer shall determine the admissible values of "P_1" and "P_2" or in fact the admissible residual pulsation in the circuit**.** We don't recommend them to be less than +/- 2%, as the environmental temperature conditions will very probably modify the theoretical calculation.

MOUNTING SUGGESTIONS FOR MAXIMUM DAMPENER EFFICIENCY

As we have seen so far, taking into consideration the flow curves for the three types of pump (flow curve graphs in **Figure 4**), the single piston pump is the pump with the higher "**maximum instantaneous flow / mean flow**" ratio and also the one with highest liquid fluctuation inside the dampener in each cycle, "**δV**" if we consider the same piston diameter and stroke length for all three pumps. Therefore in the next example we will refer to the one piston single acting pump.

We can assume that for **99%** of industrial applications, if the recommendations that we detail below are followed, the dampener's efficiency will be guaranteed.

For pulsation dampeners with one (1) unique connection port, ***HIDRACAR S.A.*** recommends installing the dampener with its axes aligned with the pipe discharge line, and the rest of the pipe downstream the dampener in a T derivation, see next **Figure 6**.

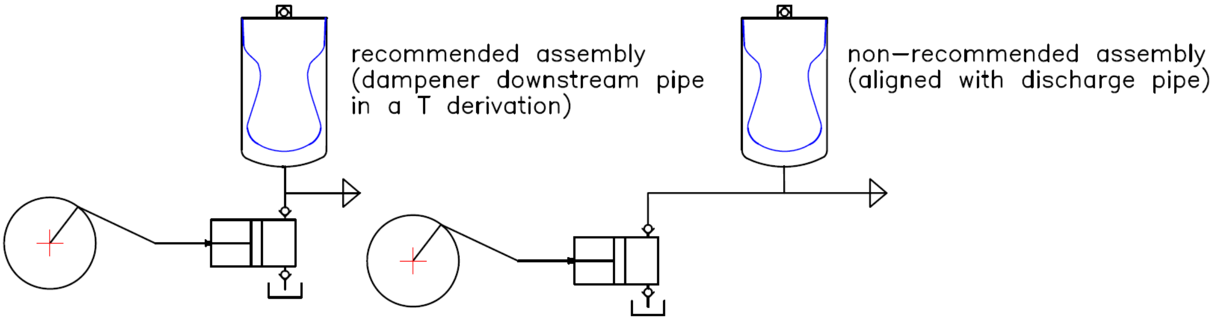


Figure 6. Scheme for the recommended installation of a discharge pulsation damper with one (1) single connection port.

1.- The dampener must be mounted with its axis aligned with the axis of the pump outlet.

2.- The distance between the pump outlet port and the dampener port connection must be as short as possible.

3.- The pipe section between the pump and the dampener connection must be calculated for the pump maximum instantaneous flow.

4.- The remaining pipe section downstream the pulsation dampener shall be conducted with a T derivation. This dampener downstream pipe must be calculated for the mean flow.

In the scheme of **Figure 7** we will see more clearly all the concepts we have exposed so far.

ω : Pipe section for the mean flow.
Ω : Small length of pipe section for the maximum instantaneous flow.
Q : Maximum instantaneous flow.
q : Mean flow.
L : Distance between pump and dampener, as short as possible.

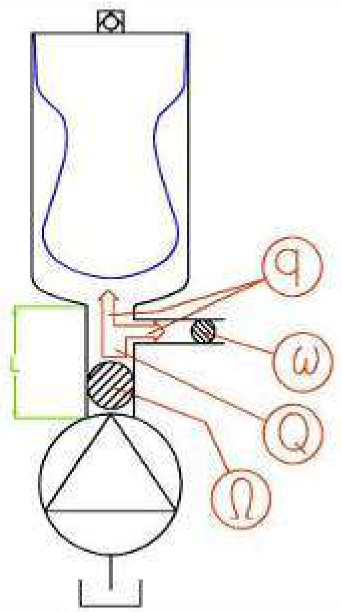


Figure 7. Scheme of the main parameters involved in the in-line assembly of a pulsation dampener.

In order to illustrate the difference between the two pulsation dampener installation schemes in **Figure 6** into a circuit, and the higher efficiency that represents installing the pipe downstream the dampener in a T derivation, we will remember some fluid mechanics principles:

The flow of a liquid inside a pipe follows different speed lines. In the centre of the pipe the velocity is maxim while it becomes nearly to zero close to the pipe inner wall (see next drawing). If the mean liquid velocity increases, the difference between dynamic pressure (pressure measured in the liquid movement direction) and static pressure (pressure measured perpendicular to the liquid movement direction) also increases.

The scheme of **Figure 8** reflects this phenomenon: dynamic pressure reading (B) is the higher pressure and it is achieved in the dampener connection port of recommended installation (**Figure 6 left**); static pressure reading (A) is the lower pressure and it is achieved in the dampener connection port of non-recommended installation (**Figure 6 right**).

In fact, the alignment of the flow with the dampener connection port facilitates the entrance of the liquid in the damper due to its higher dynamic pressure. *(Note: We assume the fluid circulates in a laminar regime)*

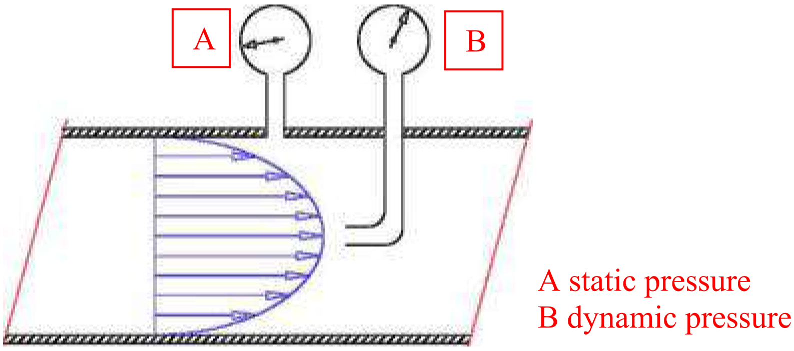


Figure 8. Scheme of the dynamic pressure in a pipe cross section

If the dampener is far from the pump outlet, the efficiency of the dampener will be reduced a great deal. And if on top of this, the dampener having one (1) single connection port is installed aligned with the pipe (as per scheme of **Figure 6 right**) and the pipe derivation conducting to the dampener have a smaller diameter than the main circuit pipe, then the effect of the dampener will be negligible.

HIDRACAR S.A. has available different IN-LINE solutions for pulsation dampeners with flow passing through (see on scheme of **Figure 9**). Those designs are specially indicated for those applications which require an installation as per scheme in **Figure 6 right** (for example: horizontal discharge pipes, collectors of multi headed pumps, etc).
In those dampeners, all the circuit flow passes through the dampener interior. Those dampeners have been specially designed to improve the dampening efficiency when installed aligned with the discharge piping.

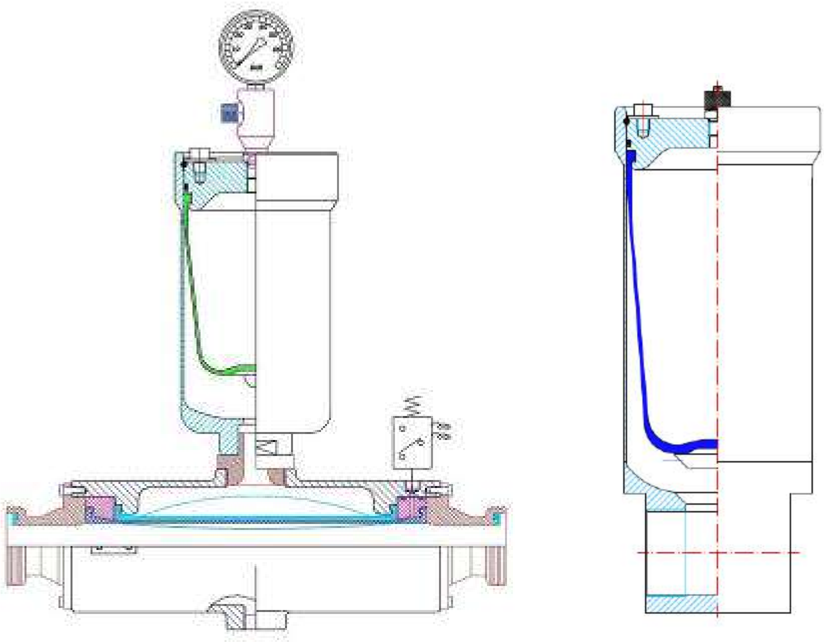


Figure 9. On the left, IN-LINE hygienic dampeners. On the right, BLADDER dampeners with 2 connection ports

WARNING¡: It is of utmost importance that the pulsation dampener hole passage must be as similar as possible than its connection port and the pipe section. Any reduction in the diameter of the hole passage, in dampeners installed in low pressure circuits, will greatly reduce the performance and efficiency of the dampener.

SOLUTION TO PROBLEMS OF PARTICULAR PULSATION DAMPENER APPLICATIONS

I) CIRCUITS THAT HAVE TO BE CLEANED PERIODICALLY AT THE END OF EACH PROCESS

Our NEW IN-LINE tube pulsation dampers (see on scheme of **Figure 9**), thanks to its special design without corners, can be cleaned in place using CIP processes (a cleaning agent is pumped in the circuit at certain pressure and temperature to clean all pipes and wetted elements in the circuit).

All the rest of pulsation dampers, though certainly some more than others, have internal corners which are hard to reach and difficult to clean or totally eliminate the residues of the pumped product with a CIP process.

The most reliable, low cost and efficient solution to this problem, in accordance with our longer than 45 years experience, is to use our quick dismantling system for bladder dampeners, to extract the bladder out of the dampener, and then clean separately both the bladder and the interior of the dampener body. In the case of applications where the charging gas pressure is lower than **10 bar** and compressed air can be used to fill the dampener, it is the most effective solution. ***HIDRACAR S.A.*** has designed a quick bladder dismantling system that makes unnecessary any additional tool.

If for whatever the reason, dismantling the bladder is not possible, we recommend the pressure of the cleaning liquid to be higher than the pumping pressure of the process product. That way the bladder or membrane will be more compressed, allowing a better access of the cleaning fluid in the internal corners in between the bladder/membrane and the dampener inner wall.

II) CIRCUITS WITH A VARIABLE WORKING PRESSURE

The problem arisen by the application of dampeners to this type of circuits has different solutions. But also in this case the experience has shown us that the best solution is, as always, the simplest one, or at least the solution requiring a lower implementation and maintenance cost and no extra energy.

Let's consider the following example: A circuit that must work at an initial pressure of **20 bar** and a final pressure of **200 bar**, with a **δV = 15 c.c.** and an admissible residual pulsation at **200 bar** of **+/- 5%** (*****). The pump type is 1 piston single acting and its capacity per stroke is: **30 c.c.** To simplify the calculations we will consider that the gas volume variation takes place at a constant temperature (isothermal curve complying with **P x V = Constant**).

((*): At 20 bar the residual pulsation will be much lower because, as shown below, the dampener size is calculated for the maximum circuit pressure and therefore when the circuit is working at the minimum pressure - here, 20 bar - the gas inside the dampener will expand and consequently the residual pulsation will decrease from the +/- 5% initially admitted).

Since: $\mathbf{P_2 \times V_2 = P_0 \times V_0 \quad P_0 = 0.8 \times 20 = 16\ bar \quad P_2 = 200 + 5\% = 210\ bar}$

$$\mathbf{P_2 / P_0 = V_0 / V_2 = 210 / 16 = 13.13} \quad (8)$$

We will calculate the volume of a hypothetical dampener for the maximum pressure of **210 bar**.

$$\mathbf{\underset{\text{(at 200 bar)}}{V_0} = (210 \times 15) / [0.8 \times 0.8 \times (210 - 190)] = 246.09\ c.c.} \quad \text{(from formula (7) in page 4)}$$

This volume is equivalent to "$\mathbf{V_2}$" from the equality (8), and consequently:

$$\mathbf{(210 / 16) = (V_0 / 246.09) = 13.125}$$

and

$$\mathbf{V_0 = 246.09 \times 13.125 = 3{,}229.98 c.c.}$$

This is in theory the total dampener volume necessary for this application; nevertheless, the ratio, $\mathbf{V_0 / V_2}$ cannot be higher than **4** (In bladder type dampeners. The value will be different in other design types of dampener. Please, consult ***HIDRACAR S.A.*** technical department for further details on the particular) in order not to wrinkle the bladder excessively, what could tear it prematurely. In our example, we have a ratio $\mathbf{V_0 / V_2}$ of **3,229.98 / 246.09 =13.125**, more than **3** times higher than the value of **4** that we have just recommended.

To avoid exceeding this ratio of **4:1**, a certain amount of liquid must be introduced inside the bladder together with the gas (usually the same liquid of the circuit or any other unable to react with either the bladder material or with the circuit liquid). Again, in our example this volume of liquid which has to be introduced into the bladder, **"V_L"** (see the scheme in **Figure 10**), is calculated:

$$\mathbf{(3{,}229.98 + V_L) / 246.09 + V_L) \leq 4} \quad \text{and operating:} \quad \mathbf{V_L = 748.54\ c.c.}$$

The total dampener volume needed will be: **3,229.98 + 748.54 = 3,978.52c.c.**

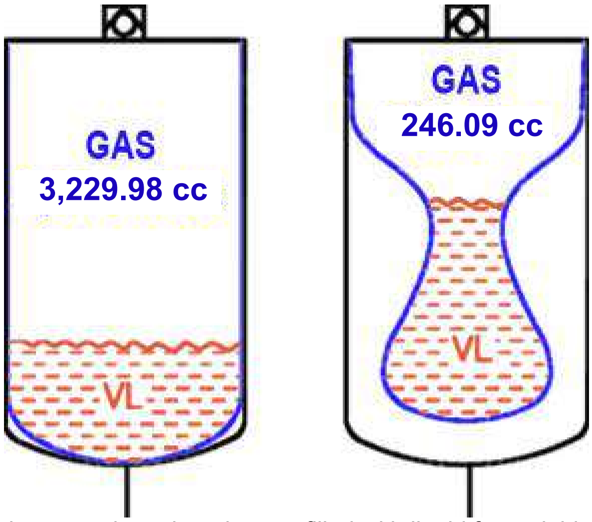


Figure 10. Scheme of the gas volume in a damper filled with liquid for variable pressure applications.

WHEN TO INSTALL A PULSATION DAMPENER AT THE SUCTION INLET OF A VOLUMETRIC PISTON PUMP TYPE OR SIMILAR DOSING PUMPS

As already said, volumetric pumps are used to dose with precision a constant volume of liquid. And therefore, the pump must get completely filled in every suction stroke piston displacement cycle.

When in the liquid inlet port of the pump the pressure can easily overcome the resistance of the suction valve spring that all pumps have (we can assume that it happens when the pressure at the inlet port to exceeds the resistance of the valve spring more than 3 bar) and the section of the suction pipe is about twice the discharge section of the pump, it won't be necessary to install a pulsation dampener at the suction inlet.

If the static pressure of the liquid at the pump inlet is low (below the already mentioned 3 bar) the suction pipe is long enough (longer than 3 to 5 metres from the suction liquid supply tank to the pump inlet) and also the liquid has a low vapour tension at the working temperature then a phenomenon called "**cavitation**" could take place.

When this anomaly takes place, the pump could suction a mix of liquid and its vapour. When this mixture (liquid and vapor) is compressed during the pump discharge cycle causes the condensation of the vapour because of the pump impulsion pressure. Consequently there is a reduction in the volume delivered in the outlet of the pump and witch performance loses efficiency. This effect, which can be detected by a soft explosion-like sound, reduces considerably the life of the pump, which also stops providing the required dosing.

In order to eliminate this problem it is necessary to prevent the pressure at the pump inlet port to be lower or close to the vapour tension of the liquid. And a condition for this, other than having enough pressure, is to avoid the suction pipe liquid column to be subjected to accelerations and decelerations caused by the operation of the pump.

It is precisely, **and exclusively to avoid these fluctuations in the liquid column** (accelerations and decelerations) at the suction pipe, **that a pulsation dampener is needed at the suction** of volumetric or dosing pumps in the above mentioned situations.

The pulsation dampener installed at the suction of the pump fulfills the same task as the one installed at the discharge: To keep the velocity of the liquid as constant as possible; and therefore, its pressure. If the low pressure of the liquid at the suction does not experiment any substantial drop, the possibility of reaching the vapour tension of the liquid will decrease and the main cause for the appearance of "**cavitation**" will be eliminated.

The pulsation dampener will not be able to avoid the "**cavitation**" phenomenon if all its determinants are present; and therefore it is convenient, when a risk exists, to install an auxiliary centrifugal or similar pump, or else, to raise the liquid supply tank or pressurize it and this way increase the pressure at the inlet port of the dosing pump.

If all these recommendations can't be applied, there is the possibility of installing the pulsation dampener to try to avoid the appearance of the "**cavitation**" effect. For this it is specially recommended that:

The size or volume of the dampener installed at the suction must be approximately twice as much as for the one installed at the discharge.

The size of the connection port of the dampener shall be as similar as possible as the diameter of the suction pipe.

The dampener must be installed as close as possible to the pump liquid inlet port, with the least possible pipe length in between.

If the suction pressure in the pump inlet is lower than atmospheric pressure (< 1 bar), then the gas volume inside the suction damper shall be reduced. When the dampener is delivered, the bladder must be compressed with hands with internal pressure of 1 bar.

*Currently **HIDRACAR S.A.** has designed a very effective in-line bladder damper (see in our BDOS catalogue ref. BLADDER IN LINE S.S.LOW PRESSURE PULSATION DAMPENERS), that can be considered the unique suction dampener with efficiencies nearly to 100%.*

For further detail explaining about the above exposed, please, contact ***HIDRACAR S.A.*** technical department.

We have written this paper in the modest hope of helping any people interested in these devices to understand the applications of the hydro-pneumatic accumulators used as pulsation dampeners. If it results useful to anyone, we will feel satisfied and rewarded for the time and effort spent in the making.

10th rev., April 2022

Manuel Carcaré Gimeno
Technical Director & ***HIDRACAR S.A.*** founder
In collaboration with:
Eduard Cortina Ruiz
Manager Assistant in ***HIDRACAR S.A.***

HIDRACAR S.A.

ADVANTAGES AND DRAWBACKS OF USING PULSATION DAMPENERS EITHER WITH OR WITHOUT SEPARATOR ELEMENT BETWEEN FLUIDS (GAS / LIQUID)

As we already know, the volumetric or dosing pumps manage to supply a constant volume in time, but produce an oscillating and variable flow in pumps with a crankshaft movement.

As already exposed in our article *“Technical and practical considerations on the use of pulsation dampeners in circuits with volumetric or dosing pumps”*, this oscillating flow supply effect is more significant in the case of single-piston pumps; and it is in this type of pumps where the installation of a pulsation dampener becomes more useful and necessary, both at the discharge and the suction.

In some cases there is the tendency to install at the suction a dampener without a separator element between the pumped liquid and the atmospheric air inside the dampener. We understand that this solution creates a major problem that we will try to explain.

When the dampeners without separator are used at the discharge, the problem gets reduced in part.

Let’s see which are the main problems of installing such a pulsation dampener at the suction of the pump:

I) It must be always mounted upright and must be filled with the pumped liquid at least to half of its volume, leaving the remaining volume for atmospheric air. This is a hazardous operation if the liquid is corrosive, as it must be performed on site.

II) The usual problem, but even more pronounced at the suction: The atmospheric air gets dissolved as time goes by, so it becomes necessary to proceed as in (I). But, ABOVE ALL, the dissolved air reduces the dosing of the liquid the pump is providing. The pump chamber gets full of liquid and dissolved air bubbles. These bubbles, which on entering the pump have a non-negligible size, as they could be slightly below the atmospheric pressure, when the pump starts the discharge and the pressure rises get compressed, what reduces the volume of the pump head and consequently an effect akin to CAVITATION happens (*).

(*): The volume freed by the reduction of the size of the air bubbles, is filled by the pumped liquid vapour and if this circumstance does not occur the problem gets worse.

III) Comparative analysis of volumes and costs of the dampeners with and without a separator between fluids (air / liquid):

DATA OF A HYPOTHETICAL CASE (simple-effect membrane pump)

Q = 5 L/min. at 100 r.p.m.
Pumping pressure: 4 bar-g
Suction pressure: 1 bar-g
Residual pulsation admitted at the discharge: +/- 6%
Residual pulsation admitted at the suction: +/- 3%

THEORETICAL CALCULATIONS ON THE VOLUME OF THE DAMPENER AT THE DISCHARGE

With separator (bladder, membrane, bellows):

$\partial V = (5 / 100) / 2 = 0.025$ litres ≡ 25 c.c. (this is the volume that gets in and out of the dampener in each pump cycle.

$\underline{V_0} = (\partial V \times P_2) / [0.8 \times 0{,}8 \times (P_2 - P_1)] = (25 \times 4.24) / (0.64 \times 0.48) \approx \underline{345}$ c.c. (this is the total volume of the dampener).

P_2 = Working pressure plus percentage of residual pulsation = $= 4 + (6 \times 4 / 100) = 4.24$ bar

P_1 = Working pressure minus percentage of residual pulsation = $= 4 - (6 \times 4 / 100) = 3.76$ bar

Without separator:

$V_0 \times 1 \text{ at} = V_1 \times P_1 = V_2 \times P_2$

V_2 = Volume of atmospheric air inside the dampener when compressed at P_2 pressure

$P_0V_0 = 1 \text{ at} \times V_0 = P_1V_1 = P_2V_2$;

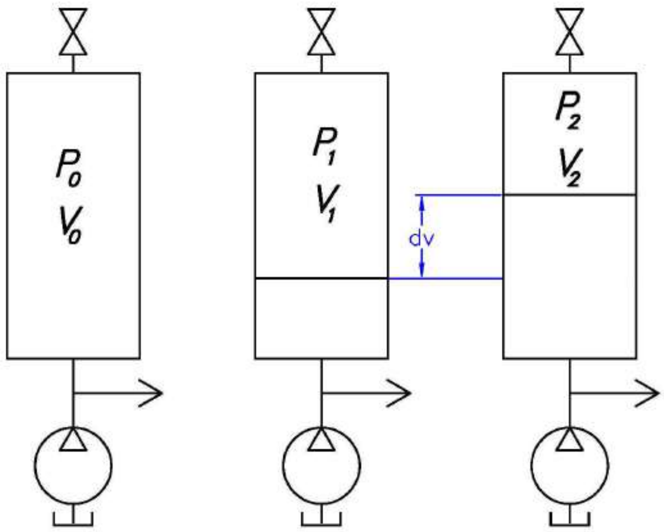
$V_1 - V_2 = \partial V = 25$ c.c., $V_1 = 25 + V_2$;

$P_1 \times (25 + V_2) = P_2 \times V_2$;

$(3.76 \times 25) + 3.76 \times V_2 = 4.24 \times V_2$;

$V_2 \times (4.24 - 3.76) = 3.76 \times 25$;

$V_2 = 94 / 0.48 \approx 195.8$ c.c.



$V_0 \times 1 \text{ at} = P_2 \times 195.8 = 4.24 \times 195.8$;
$V_0 = (4.24 \times 195.8) / 0.8 \approx 1{,}038$ c.c.!!;
1,038 / 345 = 3 times the volume of the dampener without separator compared to the dampener with separator!!!

NOTE: The higher the working pressure, the bigger the size of the dampener without separator.

CALCULATIONS OF THE DAMPENER AT THE SUCTION

With separator:

$V'_0 = \partial V \times P'_2 / (0.8 \times 0{,}8 \times (P'_2 - P'_1)) = (25 \times 1.03) / (0.64 \times 0.06) = 670.58$ c.c.
$P'_2 = 1 + [(3 \times 1) / 100] = 1.03$
$P'_1 = 1 - [(3 \times 1) / 100] = 0.97$

Without separator:

$P'_1 \times (25 + V'_2) = P'_2 \times V'_2;$
$(0.97 \times 25) + 0.97 \times V'_2 = 1.03 \times V'_2;$
$0.06 \times V'_2 = 0.97 \times 25;$
$V'_2 = (0.97 \times 25) / 0.06 \approx 404.16$
$V'_0 \times 1 \text{ at} = P'_2 \times 404.16;$
$V'_0 = (1.03 \times 404.16) / 0.8 = 520.36$ c.c.

The volume of the dampener must be at least twice the calculated value in order to get the initial level of the liquid as far from the dampener connecting port as possible. Therefore, this volume would be 520.36 x 2 = 1,040.72 c.c.

Summarizing:

The main drawback of not using pulsation dampeners with separator, either at the suction or the discharge, is the dissolving of the air inside the dampener into the liquid and the need for stopping the pump regularly to refill the dampener with atmospheric air; with the recurrent hazardous exposure in case of pumping corrosive chemicals.

But above all, in the application of the dampener without separator at the suction of the pump, the dissolving of air into the liquid can create cavitation and a deficient dosing.

The use of dampeners without separator, either at the suction or the discharge, will require dampeners with a bigger size than those needed if fitted with a separator.

FEBRUARY 2019

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UNQUESTIONABLE BENEFITS OF INSTALLING A PULSATION DAMPENER AT THE DISCHARGE OF SINGLE-EFFECT DOSING PUMPS

As we have already seen, all single effect dosing pumps does not supply any flow during the filling or suction cycle of the pump. This means that at the end of such cycle, the pumping pressure has been reduced to "zero". The liquid column inside the discharge pipe has stopped.

On starting the course of discharge or the exiting of the liquid from the pump, the liquid column must overcome:

a) The inertia of the mass of the liquid that has stopped.

b) The resistances that are generated in the circuit against the movement of the liquid. These resistances are:

  I) Geometrical height.

  II) Head loss.

CONSEQUENTLY, the pressure at the outlet of the pump goes from "zero" to a pressure generated by resistances *a* and *b*.

This variation of pressure, from "zero" to a maximum value, creates the following problems:

- Fatigue of the material of the pump mechanisms, piping, filters, flow meters, threaded or flanged couplings, etc…
- Vibrations that end up producing leaking of the liquid at the couplings.
- The impossibility of getting a precise reading of the flow meter.

All this shows how necessary is the installation of a pulsation dampener to avoid all the problems that have been exposed. As the dampener procures a more constant flow in the pipe, it is possible to calculate more accurately its section and it always results in a diameter reduction. This alone already redeems in part the extra cost assumed on installing the dampener.

Let's see now how we can reduce to a certain extent the cost of the dampener.

As we already know, every time the size of the dampener must be calculated it is necessary to know the residual pulsation percentage that can be admitted or tolerated in the circuit. The final customer always tends to reduce this value when asked about, even though in most cases it is not necessary to adjust it to such tight values. In any case the pumping pressure must always be taken into account (it is not the same a wide percentage for a low pressure, say 6 bar than for a pressure of 200 bar or higher).

A simple illustration will make evident the reduction in the size of the dampener, just increasing slightly the percentage of residual pulsation (for a single piston pump):

If the pump head: 50 c.c.
The pumping pressure is: 6 bar
The initial residual pulsation is: +/- 4%
The size of the dampener will be:

$V_0 = (\partial V \ x\ P_2) / 0.64 \ x\ (P_2 – P_1) = (25 \ x\ 6.24) / (0.64 \ x\ 0.48) = 498.29$ c.c.
V_0 = Dampener size.
∂V = Volume of liquid the dampener will store and return = pump head / 2 (for single piston or membrane pumps)
$P_2 = 6 + (4 \ x\ 6 / 100) = 6.24$ bar
$P_1 = 6 - (4 \ x\ 6 / 100) = 5.76$ bar

If we take a pulsation % of +/- 8%

$P'_2 = 6 + (8 \ x\ 6 / 100) = 6.48$ bar
$P'_1 = 6 - (8 \ x\ 6 / 100) = 5.52$ bar
and $V'_0 = (25 \ x\ 6.48) / (0.64 \ x\ 0.96) = 258.68$ c.c.

We then see that if we change from a +/- 4% residual percentage to a +/- 8%, the size of the dampener has been reduced to approximately by half.

Pressures will fluctuate, with a 4%
+6.24; -5.76
and with a 8% residual pulsation
+6.48; -5.52
the fluctuation is just +/- 0.24 bar (difference between 6.48 – 6.24 = 0.24).

In a few words with a higher residual pulsation percentage (8%) the pressure fluctuation in the circuit is of just:
+6.48 bar; -5.52 bar (for a theoretical pumping pressure of 6 bar)

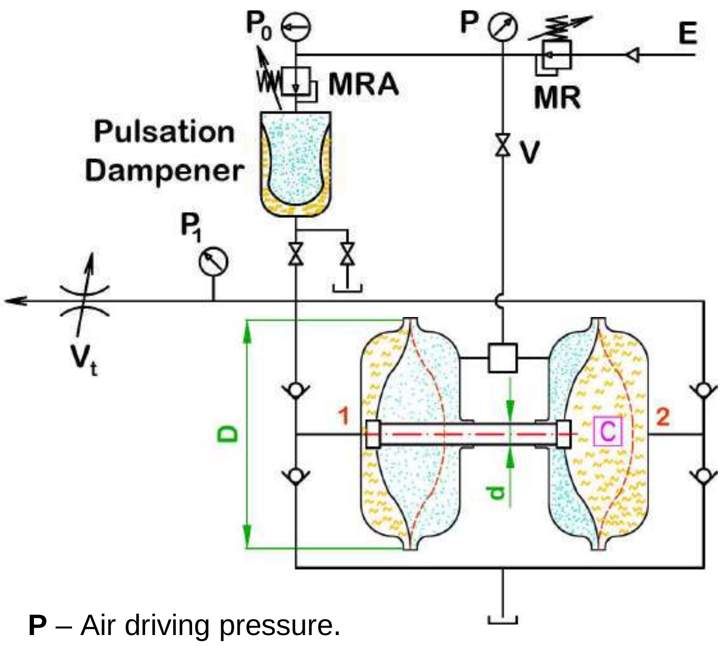
FINAL SUMMARY

In the single-effect dosing pump application, what is important is avoiding the fluctuation of the pump discharge pressure from “zero” to a maximum as it will eventually generate breakdowns in the circuit.

Therefore and unless the final customer wants to control with great precision the pressure fluctuation, ***HIDRACAR*** recommends, for these working pressure values (below 10 bar) to calculate the dampener size with a percentage of +/- 8% in order to avoid an important extra cost of the pump + dampener combination.

FEBRUARY 2019

PULSATION DAMPER APPLICATION ON AN AIR VARIABLE PRESSURE DRIVING MEMBRANE PUMP



E – *Compressed air from the factory circuit.*
MR – *Air pressure reducer.*
MRA – *Dampener air precharging pressure reducer.*
V – *Isolating valve.*
V_t – *Throttle valve to increase the dampener efficiency.*

START RUNNING INSTRUCTIONS

I) Valve "V" closed. Fill the Dampener with air at an estimated pressure. Follow the formulas beside.

II) Open Valve "V" and adjust the working pressure needed in the liquid circuit.

III) With the air reducer valve "MRA" adjust the entrance of air into the Dampener until the pressure gage reads the accepted or calculated residual pulsation pressure.

P – Air driving pressure.
P_1 – Liquid pumped pressure.
P_0 – Dampener precharging air pressure.

$$P \times (D-d)^2 = P_1 \times D^2$$

NEVER start pumping liquid without air inside the dampener. The Bladder, Membrane or Bellows of the Dampener can be damaged.

$P_1 = [P \times (D-d)^2] / D^2$; $(D-d)^2 / D^2$ = PUMP CONSTANT = K

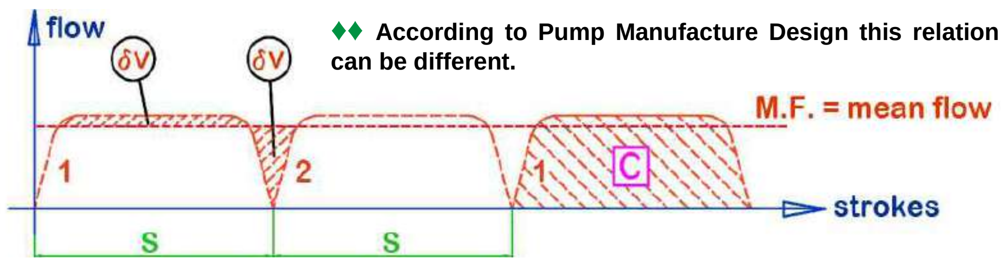
$P_0 \approx 0.75 \times P_1 \longrightarrow \boxed{P_0 \approx 0.75 \times P \times K}$

NOTE: P_0 ought to be measured with the dampener empty of liquid.

P_1 versus P_0 @ Constant Temperature	
P_1	**P_0**
8	6
7	5
6	4.5
5	3.5
4	3
3	2
2	1.5
1	0.7

∂V - *Liquid going into / out the dampener.*
C – *Liquid volume pumped per stroke.*
S – *Pump stroke.*

♦♦ Relation between **C** and **∂V**: $\boxed{\partial V \approx 0.2 \times C}$



♦♦ According to Pump Manufacture Design this relation can be different.

FORMULA TO CALCULATE THE PULSATION DAMPER SIZE (V_0)♦ :

$$\boxed{V_0 \approx 15 \times \partial V}$$

♦ FOR A RESIDUAL OSCILLATING PRESSURE OF APPROX. +/- 5% @ CONSTANT TEMPERATURE (To reduce this percentage, increase the Dampener size or, for more accuracy, see our Pulsation Damper Technical and Practical Article)

HIDRACAR, S.A. • Pol. Ind. Bufalvent - c/ Ramón Farguell, 73-77. 08243 Manresa, Barcelona (SPAIN)
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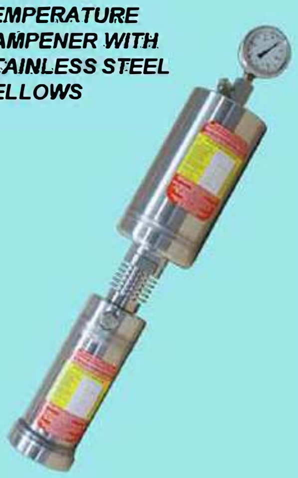

PTFE BELLOWS DAMPENER FOR CORROSIVE LIQUIDS

TWO PORT CONNECTION BLADDER DAMPENER

PTFE MEMBRANE DAMPENER

WITH ROD INDICATOR AND ANSI FLANGE

TWO PORT CONNECTION BLADDER DAMPENER FOR FOOD APPLICATIONS

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"We make liquids flow smoothly through pipes"

BLADDER, MEMBRANE & BELLOWS

PULSATION DAMPENERS

TO STABILIZE THE FLOW AND PRESSURE IN CIRCUITS WITH VOLUMETRIC PUMPS

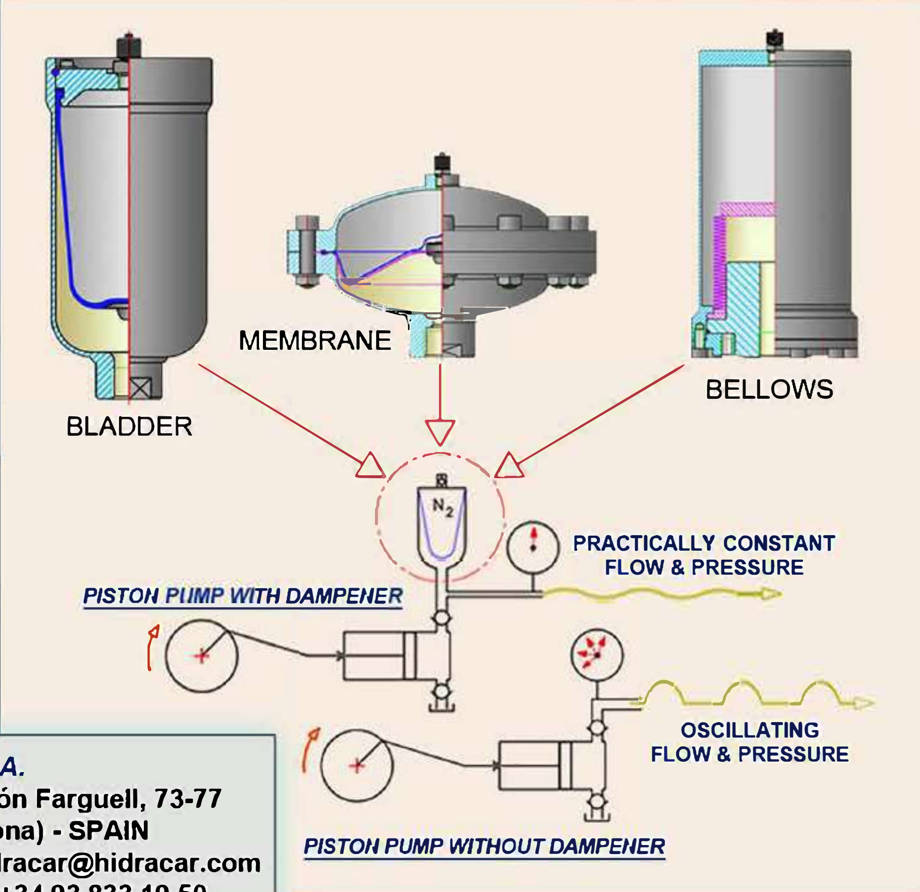
- ✓ ALLOW PUMPS TO WORK WITHOUT SHOCKS, INCREASING ITS LIFE AND THE LIFE OF FILTERS, FLOWMETERS AND OTHER ACCESSORIES
- ✓ GIVE MORE ACCURACY TO PRESSURE GAUGES AND FLOWMETERS
- ✓ PREVENT LEAKAGE IN PIPE CONNECTIONS, CREATED BY PRESSURE PEAKS

SIZES RANGE FROM 0.07 TO 35 LITRES AND WORKING PRESSURES UP TO 1,000 bar

MATERIALS:

BODY: AISI 316L, POLYPROPILENE, PVC, PVDF & OTHERS

SEPARATOR: NITRILE, EPDM, FKM, SILICONE, PTFE, STAINLESS STEEL & OTHERS



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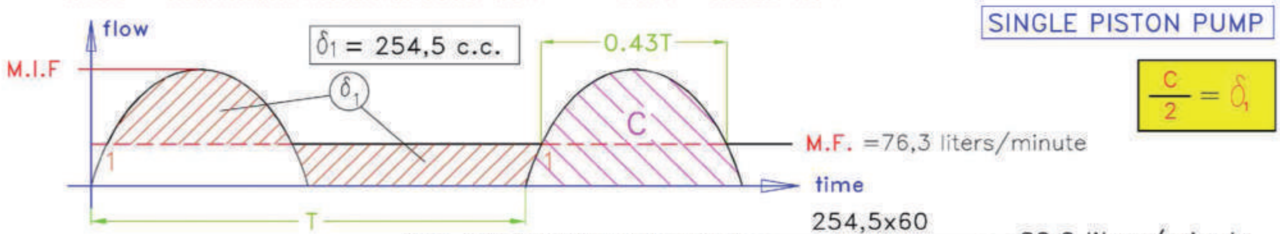
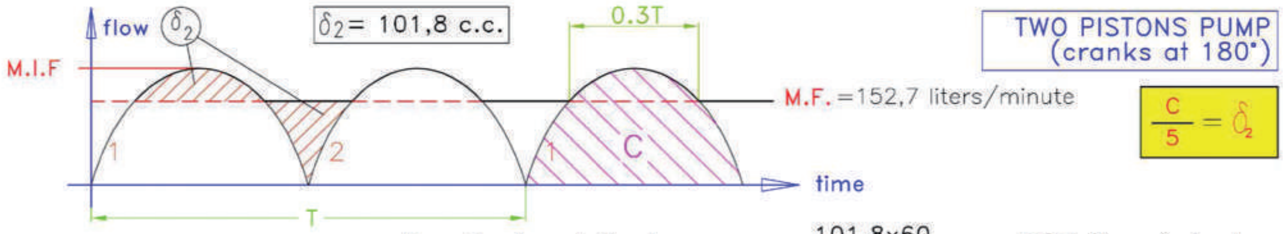
FLOW GRAPHICS OF DIFFERENT PISTON PUMP TYPES WITH A PULSATION DAMPER INSTALLED.
THE LIQUID FLUCTUATION INSIDE THE DAMPENER IS REPRESENTED

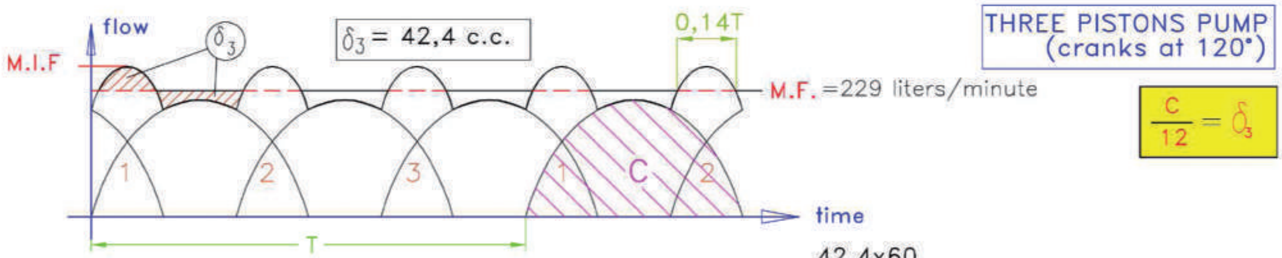
T = time employed by the crankshaft when turning one revolution (ex. 0,4 sec.=150 r.p.m.)
C = capacity of the piston head (ex. 509 c.c. for the three pump types)
δ = theoretically the amount of liquid going in and out of the dampener in each cycle
M.I.F. = maximum instantaneous flow   M.F. = mean flow



$$\text{Max. flow through the dampener} = \frac{254{,}5\text{x}60}{0{,}43\text{x}0{,}4\text{x}1000} = 88{,}8 \text{ liters/minute}$$



$$\text{Max. flow through the dampener} = \frac{101{,}8\text{x}60}{0{,}3\text{x}0{,}4\text{x}1000} = 50{,}9 \text{ liters/minute}$$



$$\text{Max. flow through the dampener} = \frac{42{,}4\text{x}60}{0{,}14\text{x}0{,}4\text{x}1000} = 45{,}4 \text{ liters/minute}$$

EASY DAMPENER SIZE SELECTION CHART ACCORDING TO THE CAPACITY PER HEAD (*) AND THE ADMISIBLE RESIDUAL PULSATION (±%)

DAMPER TYPES REF.			DAMPERNER VOLUME (liters)			1 PISTON PUMP		2 PISTON PUMP		3 PISTON PUMP	
						ADMISIBLE RESIDUAL PULSATION (±%)					
						± 3%	± 6%	± 3%	± 6%	± 3%	± 6%
BLADDER	MEMBRANE	BELLOWS	BLADDER	MEMBRANE	BELLOWS	(*) CAPACITY PER HEAD (in cc)					
U000			0,04			3	6	7	14	18	36
U001			0,09			7	14	16	32	40	80
U002	M002	F002	0,18	0,20	0,15	14	28	35	70	80	160
U003	M004	F003	0,36	0,40	0,30	25	50	60	120	150	300
U007	M008	F007	0,65	0,80	0,70	45	90	110	220	270	540
U010			0,95			70	140	175	350	420	840
U015	M012	F015	1,50	1,20	1,50	110	220	275	550	660	1320
U030	M030	F030	2,60	2,80	2,60	190	380	475	950	1140	2280
U040	M040	F040	3,80	4,00	3,80	280	560	700	1400	1680	3360
U060	M060	F060	5,60	5,60	5,60	430	860	1075	2150	2580	5160
U100	M100	F100	10,40	10,00	10,00	775	1550	1925	3850	4650	9300
U150		F150	15,00		15,00	1120	2240	2800	5600	6720	13440
U250			25,00			1850	3700	4625	9250	11100	22200

WE CAN CHANGE THE DATA WITHOUT PREVIOUS NOTICE

NOTE: THE TABLE VALUES ARE APPROXIMATE AND CORREPOND TO A CONSTANT TEMPERATURE OF THE LIQUID AND EVIRONMENT

FORMULA TO OBTAIN THE (*) CAPACITY PER HEAD

$$C = \frac{FLOW(l/h)}{n \times 60 \times s.p.m.}$$

l/h = liters/hour
n = nº of heads
s.p.m. = strokes per minute, crankshaft revolution per minute

HIDRACAR S.A.

The European nº1 providing dampening solutions
Nº1 de Europa en soluciones de amortiguación

THE AUTHENTIC AND EFFECTIVE "IN-LINE" PULSATION DAMPERS
LOS AUTÉNTICOS Y EFECTIVOS AMORTIGUADORES DE PULSACIONES "EN LÍNEA"

FOR FOOD AND PAHRMACEUTICAL PROCESSES / PARA PROCESOS ALIMENTARIOS Y FARMACÉUTICOS

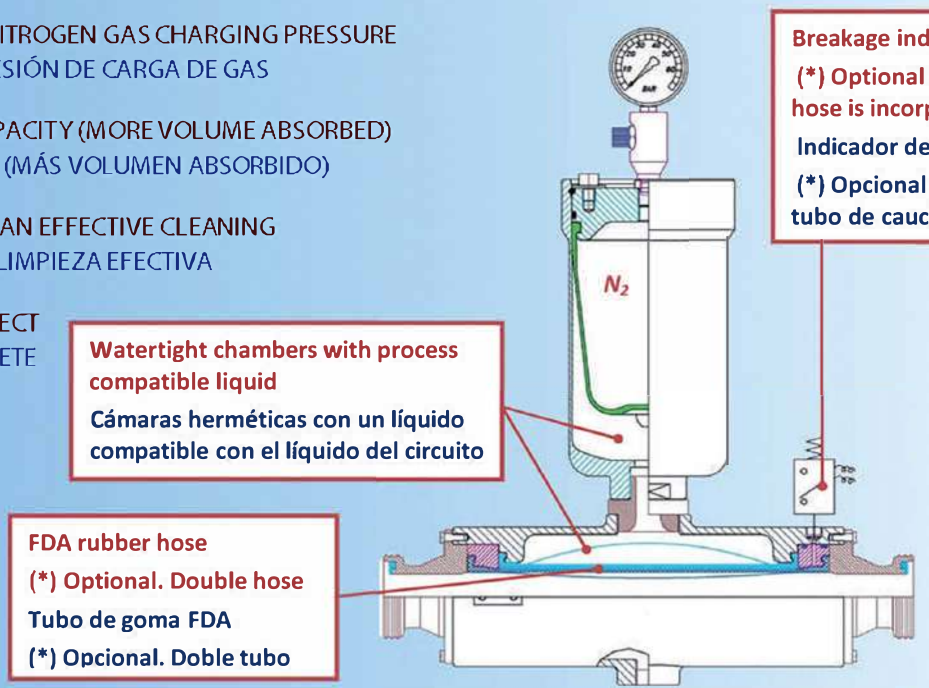
MAIN CHARACTERISTICS OF THE NEW IN-LINE DAMPER : / PRINCIPALES CARATERÍSTICAS DEL NUEVO AMORTIGUADOR "EN LÍNEA":

- NO LIMITATION IN THE NITROGEN GAS CHARGING PRESSURE
SIN LIMITACIÓN EN LA PRESIÓN DE CARGA DE GAS

- HIGHER DAMPENING CAPACITY (MORE VOLUME ABSORBED)
MAYOR AMORTIGUACIÓN (MÁS VOLUMEN ABSORBIDO)

- WITHOUT CORNERS FOR AN EFFECTIVE CLEANING
SIN RINCONES PARA UNA LIMPIEZA EFECTIVA

- NO WATER HAMMER EFFECT
SIN EFECTO GOLPE DE ARIETE

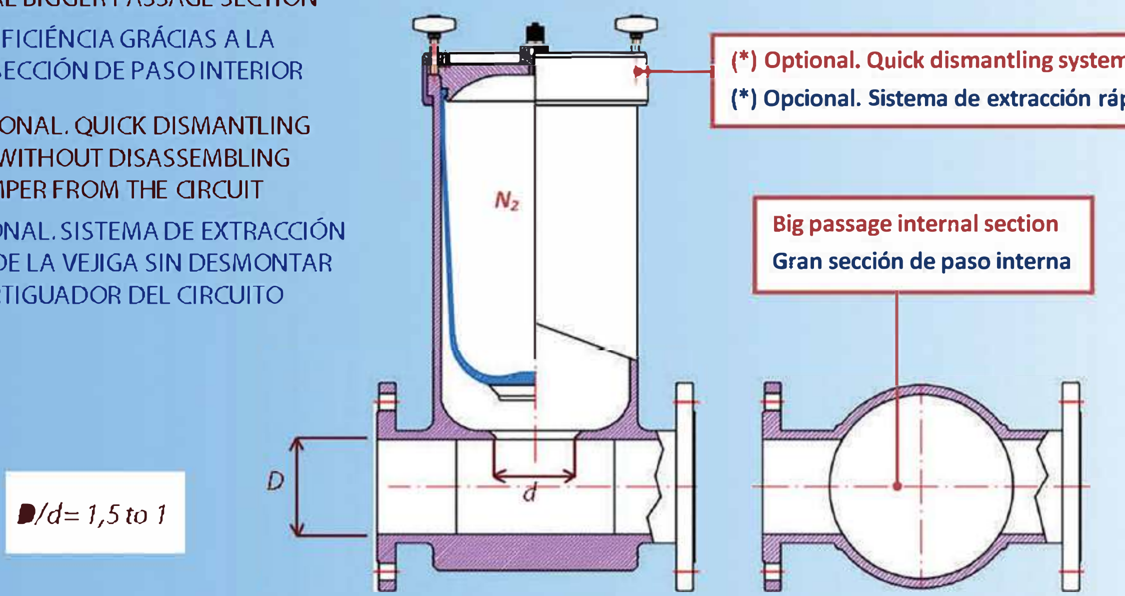


FOR PROCESSES CONTAINING SOLID PARTICLES / PARA PROCESOS QUE CONTIENEN PÁRTICULAS SÓLIDAS AND ALSO FOR SUCTION LINES / Y TAMBIÉN PARA LÍNEAS DE SUCCIÓN

- THIS DESIGN HAS BEEN TESTED BY "GRUNDFOS". THE HIGH FREQUENCY (50 Hz) PEAKS OF PRESSURE HAS BEEN REDUCED 80%
EN ESTE DISEÑO ENSAYADO POR "GRUNDFOS". LOS PICOS DE PRESIÓN A ALTA FRECUÉNCIA (50 Hz) SE REDUJERON AL 80%

- HIGHER EFFICIENCY THANKS TO THE INTERNAL BIGGER PASSAGE SECTION
MAYOR EFICIÉNCIA GRÁCIAS A LA MAYOR SECCIÓN DE PASO INTERIOR

- (*) OPTIONAL. QUICK DISMANTLING SYSTEM WITHOUT DISASSEMBLING THE DAMPER FROM THE CIRCUIT
(*) OPCIONAL. SISTEMA DE EXTRACCIÓN RÁPIDA DE LA VEJIGA SIN DESMONTAR EL AMORTIGUADOR DEL CIRCUITO



HIDRACAR S.A. • Pol. Ind. Bufalvent – c/ Ramón Farguell, 73–77 Manresa (Barcelona) - SPAIN www.hidracar.com • Tel.: +34 93 833 02 52 • E-mail: hidracar@hidracar.com

HIDRACAR

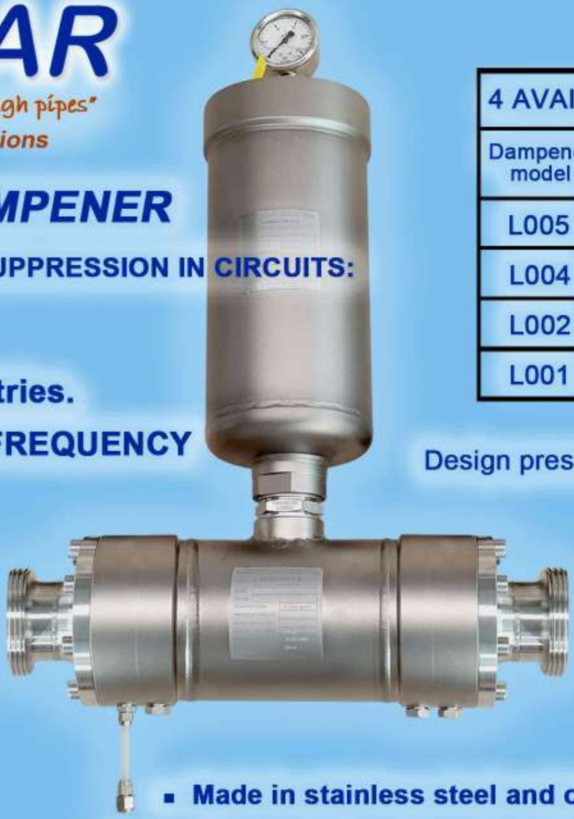
"We make liquids flow smoothly through pipes"

No. 1 providing dampening solutions

IN-LINE PULSATION DAMPENER

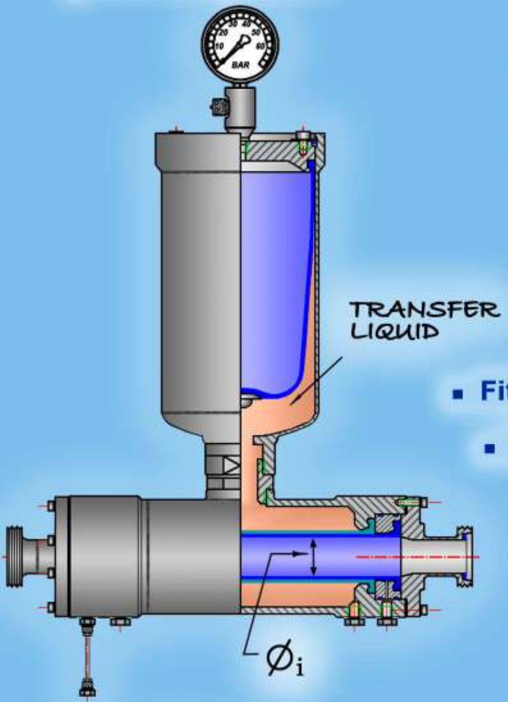
100% EFFECTIVE PRESSURE PULSE SUPPRESSION IN CIRCUITS:

- **for FOOD & BEVERAGE.**
- **for PHARMACEUTICAL industries.**
- **for circuits with VERY HIGH FREQUENCY pressure peaks.**



4 AVAILABLE SIZES	
Dampener model	Internal hose diameter ($\varnothing_i$):
L005	102 mm
L004	68 mm
L002	37 mm
L001	23 mm

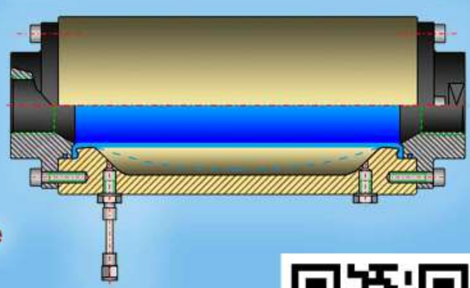
Design pressure up to 150 barg



- **Made in stainless steel and other materials.**
- **Connection ports to suit customer's requirements.**
- **Fitted with a rubber hose rupture electronic or visual indicator.**
- **With either one or two rubber hoses in EPDM, silicone, etc,...**
- **Without internal corners for a thorough cleaning.**
- **Rubbers in compliance with FDA and CE (1935/2004) regulations.**

NEW IN-LINE LOW COST PLASTIC PULSATION DAMPENERS FOR USE MAINLY IN SUCTION LINES

- **This dampener does not need gas charge; it works at the atmospheric pressure.**
- **Fitted with a rubber hose rupture visual indicator.**



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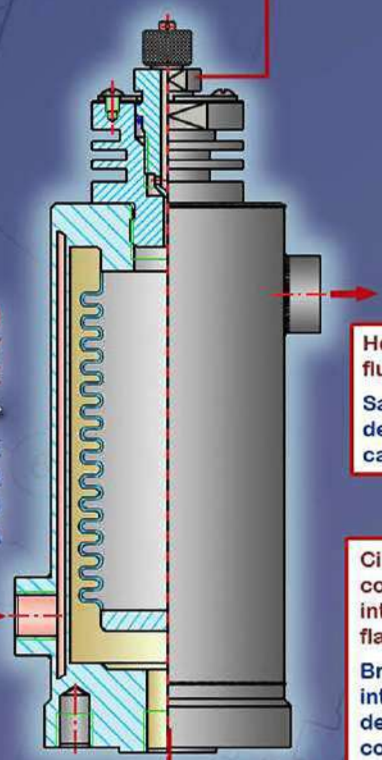
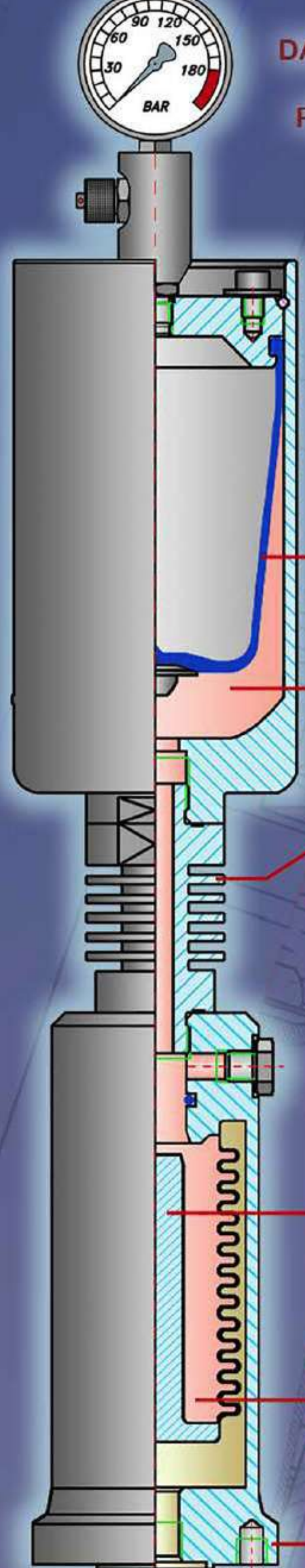
STAINLESS STEEL BELLOWS PULSATION DAMPENER

TWO SPECIAL MODELS OF DAMPENER SUPPLIED TO SEVERAL IMPORTANT GERMAN PISTON PUMP MANUFACTURERS

LOW PRESSURE DESIGN DAMPENER WITH HEATING JACKET FOR HIGH VISCOSITY FLUIDS AT A HIGH TEMPERATURE

AMORTIGUADOR DE BAJA PRESIÓN DE DISEÑO CON CAMISA CALEFACTORA PARA FLUIDOS DE ALTA VISCOSIDAD Y TEMPERATURA





AMORTIGUADOR DE PULSACIONES CON FUELLE DE ACERO INOXIDABLE

DOS MODELOS ESPECIALES DE AMORTIGUADORES DE PULSACIONES SUMINISTRADOS A VARIOS IMPORTANTES FABRICANTES ALEMANES DE BOMBAS DE PISTONES

HIGH PRESSURE DAMPENER FOR WORKING AT A HIGH TEMPERATURE AND HIGH VARIABLE PRESSURE (SEVERAL CAN BE INSTALLED IN PARALLEL, WITH DIFFERENT GAS CHARGE VALUES TO PROVIDE DAMPENING FOR A RANGE OF VARIABLE CIRCUIT PRESSURES)

AMORTIGUADOR DE ALTA PRESIÓN PARA FUNCIONAMIENTO A ALTA TEMPERATURA Y ALTA PRESIÓN VARIABLE (VARIOS PUEDEN INSTALARSE EN PARALELO, CON DIFERENTE VALOR DE CARGA DE GAS PARA PROVEER AMORTIGUACIÓN EN UN RANGO DE PRESIONES DEL CIRCUITO VARIABLES)

HIDRACAR S.A. • Pol. Ind. Bufalvent – c/ Ramón Farguell, 73 Manresa (Barcelona) - SPAIN
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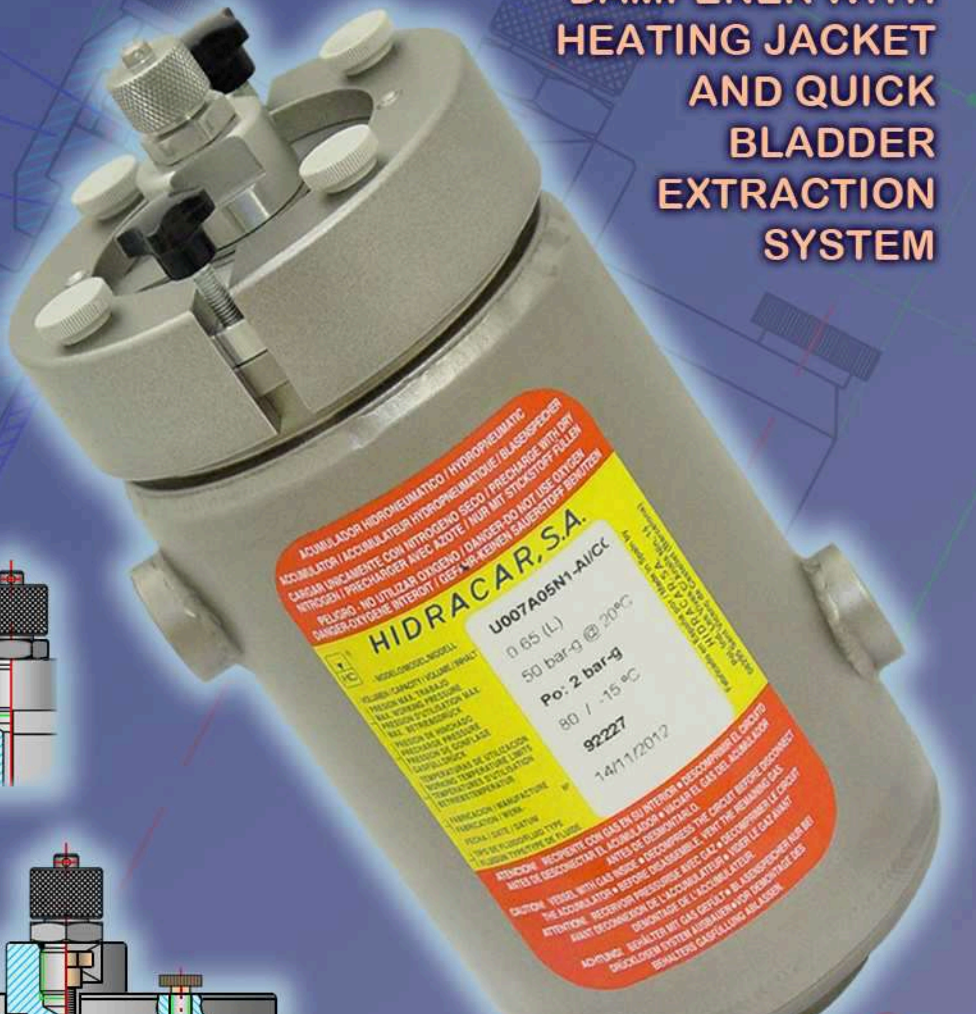
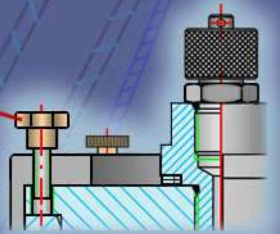
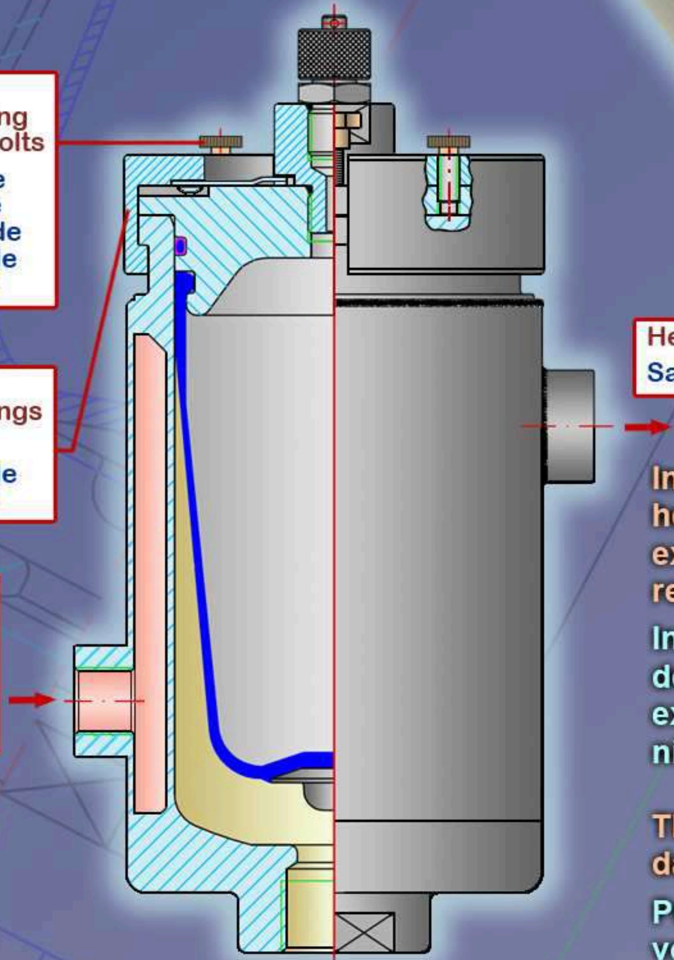
HIDRACAR S.A.

AMORTIGUADOR DE PULSACIONES DE ACERO INOXIDABLE CON CAMISA CALEFACTORA Y SISTEMA DE EXTRACCIÓN RÁPIDA DE LA VEJIGA

STAINLESS STEEL PULSATION DAMPENER WITH HEATING JACKET AND QUICK BLADDER EXTRACTION SYSTEM







Integrates both the circuit liquid heating function and the ease of extraction of the bladder without requiring any tool.

Integra la capacidad de calentamiento del líquido del circuito y la facilidad de extracción de la vejiga sin requerir ningún tipo de herramienta.

They can be made in all our standard dampener volumes.

Pueden fabricarse para todos nuestros volúmenes estandar de amortiguadores.

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HIDRACAR S.A.

HIDRACAR ACCUMULATOR REFERENCE CODE IDENTIFICATION

This is the standard ***HIDRACAR S.A.*** accumulator reference code layout (without colour; here only for code section identification purposes):

X # # # X # # X # - X X X X / X X

- The first letter (**X**) indicates the type of accumulator:

  U for bladder **M** for membrane **F** for bellows **P** for piston

- The following three digits (**###**) identify the volume of the accumulator:

U000	0.04 litres	**M008**	0.80 litres	**M040**	4.00 litres	**M100**	10.0 litres	**U250**	25.0 litres
U001	0.09 litres	**U010**	0.95 litres	**F040**	3.80 litres	**F100**	10.0 litres	**P250**	25.0 litres
P001	0.14 litres	**P010**	1.00 litres	**F040i**	3.80 litres	**F100i**	10.0 litres	**P300**	30.0 litres
U002	0.18 litres	**M012**	1.20 litres	**P040**	4.00 litres	**P100**	10.0 litres	**U320**	32.0 litres
M002	0.20 litres	**U015**	1.50 litres	**P050**	5.00 litres	**P120**	12.0 litres	**U350**	35.0 litres
F002	0.15 litres	**F015**	1.50 litres	**U060**	5.60 litres	**U130**	13.0 litres	**P350**	35.0 litres
P002	0.20 litres	**F015i**	1.50 litres	**M060**	5.60 litres	**P140**	14.0 litres	**P400**	40.0 litres
U003	0.36 litres	**P015**	1.50 litres	**F060**	5.60 litres	**U150**	15.0 litres	**P500**	50.0 litres
F003	0.30 litres	**P020**	2.00 litres	**F060i**	5.60 litres	**M150**	15.0 litres	**P600**	60.0 litres
P003	0.35 litres	**P025**	2.50 litres	**P060**	6.00 litres	**F150**	15.0 litres	**P700**	70.0 litres
M004	0.40 litres	**U030**	2.60 litres	**U061**	6.00 litres	**F150i**	15.0 litres	**P800**	80.0 litres
P005	0.50 litres	**M030**	2.80 litres	**P070**	7.00 litres	**P150**	15.0 litres	**P900**	90.0 litres
U007	0.65 litres	**F030**	2.60 litres	**P080**	8.00 litres	**P160**	16.0 litres	**P990**	99.0 litres
F007	0.70 litres	**F030i**	2.60 litres	**P090**	9.00 litres	**U200**	20.0 litres		
F007i	0.70 litres	**P030**	3.00 litres	**U095**	9.50 litres	**P200**	20.0 litres		
P007	0.70 litres	**U040**	3.80 litres	**U100**	10.4 litres	**P220**	22.0 litres		

- The second letter (**X**) refers to the type of gas charging valve: **A** for a ¼" BSP valve

- The second set of two digits (**##**) refers to the design pressure of the accumulator (number to be multiplied by 10 to give the actual pressure in bar units):

  Examples:

  02 (0)2 x 10 = 20 bar **18** 18 x 10 = 180 bar **41** 41 x 10 = 410 bar

- The third letter (**X**) identifies the material of the separator element between the charging gas (N_2 or air) and the liquid in the circuit (except for the piston accumulators, for which it identifies the material of "o"-rings):

N Nitrile rubber (NBR) **E** EPDM rubber **V** FKM rubber **B** Butyl rubber
S Silicone rubber **G** Hydrogenated NBR **R** Low temperature nitrile rubber
T TFM y PTFE **F** FKM (70% fluorine) **C** Neoprene rubber **A** Aflas **H** Hypalon
I Stainless steel **D** TFM & FKM double membrane

- Followed by a last digit (**#**) which refers to the number of connecting ports (see the standard thread size available on each technical note; these are referenced at the very end of the code as such if different from our standard thread size):

1	One connection port	**2**	Two connection ports

- Finally, the last set of two to four letters (**XXXX**) (or its absence) identifies the raw material of the accumulator body and the bladder or membrane inserts:

AI AISI 316L Stainless steel **DU** Duplex **SDU** Super Duplex **TI** Titanium
HAST Hastelloy **AC** Carbon steel **ALLY** Special alloy
SA Carbon steel – internal nickel coating accumulator for water service
PP Polypropylene **PC** PVC **PCC** Chlorinated PVC **PD** PVDF

- In some instances an extra codification for one or more special characteristics is added, separated by slashes after the basic part of the reference code:

E Special manufacture **DR** Quick dismantling design **CR** Reinforcing jacket
IN Indicator rod attachment **BA** With a connection for an additional cylinder
NS Apparatus without welded seams **IC** Internal HALAR ® coating **SB** No insert bladder
TF PTFE connection port **TFG** Graphite-PTFE connection port
PE Polyethylene connection port **PD** PVDF connection port **PC** PVC connection port
HC Hastelloy connection port **CC** With a heating jacket
(90º) Connection port at 90º **(LINIA)** In-line accumulator

Let's see an overall example:

F007A11I1-AI/CC

F007A11I1-AI/CC

F	Bellows type	**007**	0.65 litres volume
A	Fitted with a ¼" BSP valve	**11**	110 bar design pressure
I	Stainless steel bellows	**1**	One connection port
AI	Stainless steel body	**CC**	With a heating jacket

So this reference corresponds to a stainless steel, bellows type, accumulator with an internal volume of 0.65 litres, designed for working at a pressure of 110 bar, fitted with a stainless steel bellows, one standard connection port, a ¼" BSP gas charging valve and a heating jacket.

12th Rev., April 2018

ORDER REF. EXAMPLE: U007 B 01 V 1 PP

Capacity: 0.65 liter

B for Vg8, A for 1/4”BSP

01=10 bar

V= FKM Rubber Bladder

1= 1 Standard Connection port

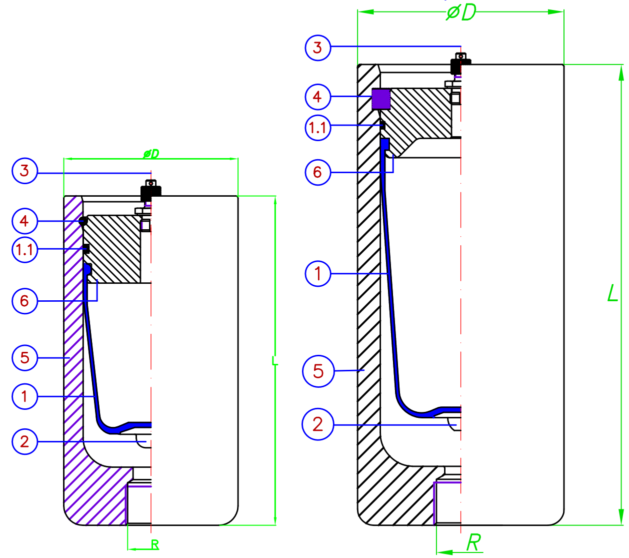
Body& insert material: Polypropylene

FOR HIGHER PRESSURES, SIZES, MATERIALS AND THREAD CONNECTIONS, PLEASE CONSULT

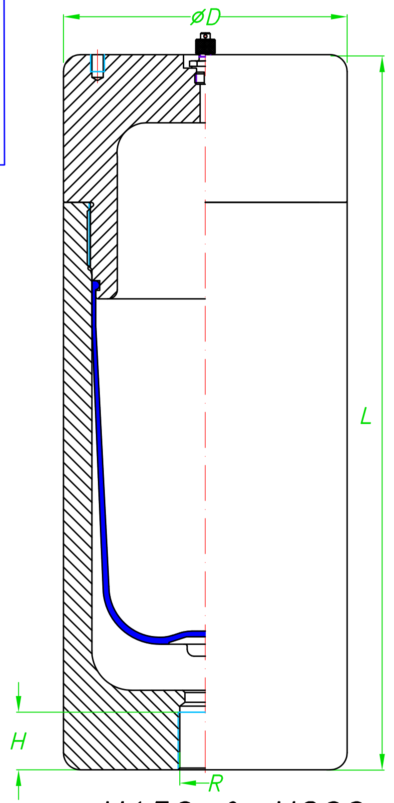
Value of ”K”: $\frac{\text{Maxi. Pressure}}{\text{Filling gas Pressure}} \leq K$ (@Constant Temp.)

** Use our PTFE + PVDF Belows dampeners

Wall thickness acc. to AD-2000 code



U000 to U100



U150 & U200

H = MAXI. LENGTH OF THREAD CONNECTION

TOLERANCES: External dimentions: ±3% Volume: +2.5% Weight: ±5%

PULSATION DAMPER REF.	VOLUME (litres)	D (mm)	L (mm)	R (BSP)	H (mm)	WEIGHT (Kg) PP	PC	PD	K VALUE
U000	0.04	60	77	3/8”	16	0.23	0.30	0.37	
U001	0.09	60	102			0.25	0.34	0.42	2.5
U002	0.18	80	140	1/2”	20	0.50	0.72	0.90	
U003	0.36	90	170	3/4”		0.68	1.03	1.26	3.0
U007	0.65	100	217		24	1.05	1.50	1.84	3.5
U010	0.95	130	242	1”	26	1.86	2.80	3.76	3.0
U015	1.50		286			2.20	3.10	4.15	3.5
U030	2.60	160	324		32	3.70	5.60	7.50	
* U040	3.80		420			4.60	6.60	8.30	
* U060	5.60	200	468	1-1/2”		8.00	11.5	**	4.0
* U100	10.40	250	493	2”	50	12.4	18.4	**	
* U150	15.00		663			16.4	24.6	**	3.0
* U200	20.00		880			21.0	27.7	**	2.0

N°	DENOMINATION	QT.	MATERIALS
6	COVER	1	(+) PP, PD or PC
5	BODY	1	(+) PP, PD or PC
4	RETAINING RING	1	(+) PP or stainless steel
3	FILLING AIR VALVE	1	AISI 316L (1/4”BSP or Vg8)
2	INSERT	1	(+) PP, PD or PC (Not included in U000)
1.1	”O”-RING	1	NBR, EPDM, FKM & BUTYL
1	BLADDER	1	NBR, EPDM, FKM & BUTYL

MAX. WORKING PRESSURE FOR ALL SIZES: 10 bar-g

MINIMUM SAFETY FACTOR: 5:1 (Minimum Rupture pressure: 50 bar-g)

Standard Bladder Rubbers: N=NBR, BUTYL, E=EPDM, V=FKM (EPDM not available for U000)

WORKING LIMITS TEMPERATURES(°C):
(0 to +60°C for PVC & PP)
(-15° to +70°C for PVDF)

(+) PC = PVC
(+) PP = Polypropylene
(+) PD = PVDF

THE MAX. WORKING TEMPERATURE CAN BE REDUCED DEPENDING ON THE LIQUID IN CONTACT

ATTENTION! THE SIZES WITH (*) ALWAYS MUST BE MOUNTED VERTICALITY (VALVE 3 ON TOP)

Those Pulsation Dampeners ought to be filled with gas at 80% working pressure. It shall be done at the working temperature.

NOTE: The precharge with N_2 or air must be done slowly and with our charging tool Ref. BVXXXA1TM connected to the 1/4”BSP charging valve

HC ® HIDRACAR SA
08243 MANRESA (BARCELONA) SPAIN
Phone: 34.93.8330252
E-mail: hidracar@hidracar.com

Customer	Customer Ref.	Replaced Drg.N°	Drawn	Approved
		AV.PL.BP.IN.DOC(Rev.20)	E.Ponsa	M.Carcaré
Title: PLASTIC PULSATION DAMPERS (standard units)		Drg.No: AV.PL.BP.IN.DOC.	Rev.: 21	Date: June-21 / Scale: none

FOR HIGHER PRESSURES, SIZES, MATERIALS AND THREADED CONNECTIONS, PLEASE CONSULT

ORDER REF. EXAMPLE: U030 B 01 V 2 PP

- Capacity: 2.6 liter
- B: for Vg8, A: for1/4"BSP
- 01≡10 bar
- V= FKM Rubber Bladder
- Two ports 2"BSP Standard Connection
- Body material: Polypropylene

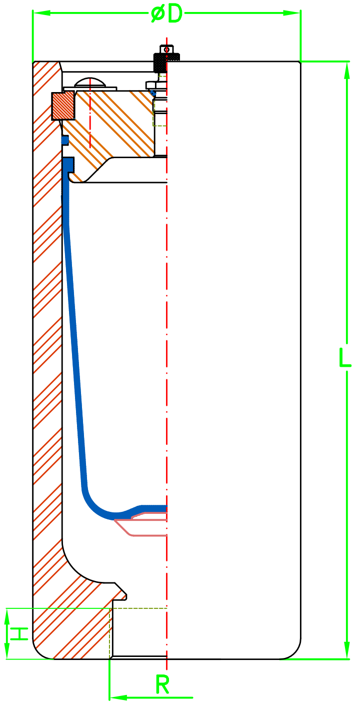
ORDER REF. EXAMPLE FOR BIG BORE: U010 B 01 V 1 PP BB

- One port 2"BSP Standard Connection
- With Big Bore connection port

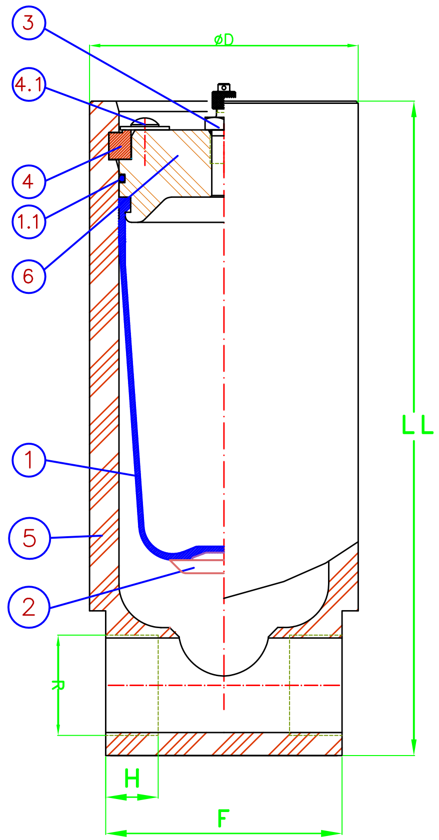
Value of "K": $\frac{\text{Maxi. Pressure}}{\text{Filling gas Pressure}} \leq$ K (@Constant Temp.)

MAX. WORKING PRESSURE: 10 BAR-G

SAFETY FACTOR: 5:1



BIG BORE



IN LINE TWO CONNECTION PORTS

PULSATION DAMPER REF.	VOLUME (litres)	D (mm)	F (mm)	H (mm)	LL	L (mm)	R (BSP)	WEIGHT (Kg) two ports	WEIGHT (Kg) BIG BORE	K VALUE
* U015	1.5	130	112.5	25	315	285	1-1/2"	2.3	2.2	3.5
U030	2.6	160	141	30	362	323	2"	4.2	3.8	
* U060	5.60	198	174.5	35	523	468	2-1/2"	8.5	7.7	4
* U100	10.4	250	221	40	578	490	4"	16.4	12	

ATTENTION! THE SIZES WITH (*) ALWAYS MUST BE MOUNTED VERTICALITY (VALVE 3 ON TOP)

TOLERANCES: External dimentions: ±3mm Volume: ±2.5% Weight: ±4%

H = MAXI. LENGTH OF THREAD CONNECTION

STANDARD BLADDER RUBBERS: N= NBR, B= BUTYL, E= EPDM, V= FKM

WORKING LIMIT TEMPERATURE(°C): (0 to +60°C,)

Note: The precharge at 80% of W.P., can be done with compressed air if it is compatible with the liquid pumped. Use a tire inflating air tool. If need to be charged with N2, use our valve Ref. 004-AI (1/4"BSP) and our charging kit BVXXXA1TM

Nº	DENOMINATION	QT.	MATERIALS
6	COVER	1	Polypropylene
5	BODY	1	Polypropylene
4.1	RETAINING BOLTS	3	AISI 316L
4	RETAINING RING	1	Polypropylene
3	AIR FILLING VALVE	1	(Vg8) AISI 316L
2	INSERT	1	PVDF
1.1	"O"-RING	1	NBR, EPDM, FKM,BUTYL
1	BLADDER	1	NBR, EPDM, FKM,BUTYL

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08243 MANRESA (BARCELONA) Spain
Phone: 34.93.8330252
E-mail: hidracar@hidracar.com

Customer	Customer Ref.	Drawn	Approved
		K.Ventura	M.Carcaré
Title: SPECIAL PP LOW PRESSURE "IN LINE" BLADDER & BIG BORE PULSATION DAMPERS FOR SUCTION LINES, PERISTALTICS PUMPS & HIGH VISCOSITY LIQUIDS	Drg.No: AV.PP.BP.DP.BB.IN.DOC	Rev.: 03	Date: July2021 / Scale: none

A02≡20bar	
A03≡30bar	
A04≡40bar	
A05≡50bar	
A18≡180bar	
A26≡260bar	

ORDER EXAMPLE: U015 A04 B 1 AI

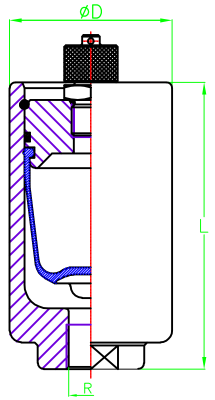
Capacity: 1.5 litres
A04≡40bar
B= BUTYL Rubber Bladder
3/4" Standard Connection
Body & insert material: AISI 316L

FOR HIGHER PRESSURES, SIZES, MATERIALS AND THREAD CONNECTIONS, PLEASE CONSULT

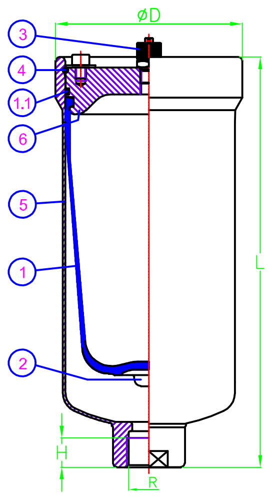
Value of "K": $\frac{\text{Maxi. Pressure}}{\text{Filling gas Pressure}} \leq$ K (@Constant Temp.)

Hydrostatic test pressure @ 1.5 * Design pressure @ 20°C

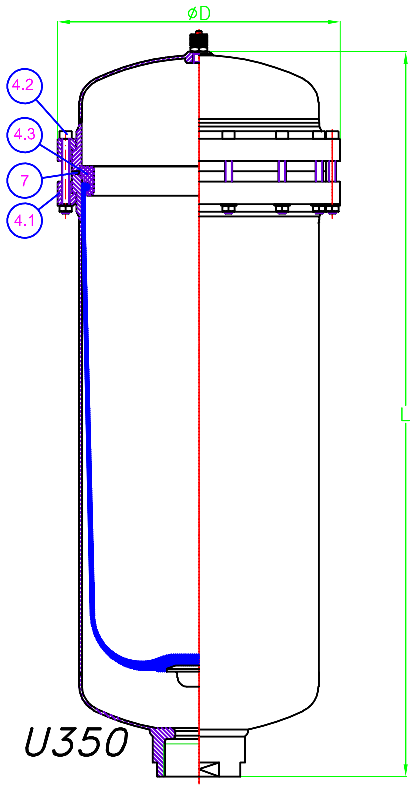
Wall thickness acc. to AD-2000 code



U000 to U003



U007 to U250



U350

H = MAXI. LENGTH OF THREAD CONNECTION

PULSATION DAMPER Reference	VOLUME (litres)	DESIGN PRESSURE (bar-g @50°C)	D (mm)	L (mm)	R (BSP)	H (mm)	WEIGHT (Kg)	K VALUE
U000	0.04	260	55	70	3/8"	14	0.8	2.5
U001	0.09			97			1.0	
U002	0.18	180	70	122	1/2"		1.8	
U003	0.36		85	168		16	3.6	3.0
U007	0.65	50	88	208	3/4"	20	2.5	3.5
U010	0.95	40	113	211		25	4.3	3.0
U015	1.50			256			4.6	3.5
U030	2.60	30	140	305	1"	27	5.3	
U040	3.80			405			5.7	5.0
U060	5.60	40	167	420	1-1/2"	30	10.0	
U100	10.40	30	217	432	2"		15.0	4.0
U150	15.00			645			19.2	5.0
U250	25.00	20	270	677	2-1/2"		26.0	4.0
U350	35.00		302	772			28.5	2.2

No	DENOMINATION	QT.	MATERIALS
7	"O" RING	1	NBR, BUTYL, EPDM & FKM
6	COVER	1	AISI 316L
5	BODY	1	AISI 316L
4.3	RETAINING RING	1	AISI 316
4.2	BOLTS & NUTS	14	DIN 912 & 934 A4-70
4.1	RETAINING RING	2	AISI 316L
4	RETAINING RING	1	DIN17224 (AISI 316)
3	INFLATING N_2 VALVE	1	AISI 316L (1/4" BSP)
2	INSERT	1	AISI 316L
1.1	"O" RING	1	NBR, BUTYL, EPDM & FKM
1	BLADDER	1	NBR, BUTYL, EPDM & FKM

ATTENTION! ALWAYS MUST BE MOUNTED VERTICALITY (VALVE 3 ON TOP)

Standard Bladder Rubbers: N=NBR, B=BUTYL, E=EPDM, V=FKM

(Other Rubbers: Neoprene, Hypalon, HNBR, etc.)	N	B	E	V
Rubbers Max. Working Temperatures (°C)	+80 −15	+100 −30	+130 −30	+200 −20

Working Temperatures versus Working Pressures **

For a temperature of	80°C	correspond design pressure	x 0.87
" " " "	100°C	" " "	x 0.82
" " " "	130°C	" " "	x 0.78
" " " "	200°C	" " "	x 0.68

TOLERANCES:
External dimentions: ±3%
Volume:±2.5% Weight:±5%

THE MAX. WORKING TEMPERATURE CAN BE REDUCED DEPENDING ON THE LIQUID IN CONTACT

Those Pulsation Dampeners ought to be filled with gas at a value of 0.80x the pressure to stabilize and that at the working temperature

NOTE: The precharge with gas or air must be done slowly and with our charging tool Ref. BV160A1TM

HIDRACAR SA®
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E-mail: hidracar@hidracar.com

Customer	Customer Ref.	Replaced Drg.N°	Drawn	Approved
		AV.AI.MP-BP.IN.DOC (Rev.23)	E.Ponsa	
Title S.S.MEDIUM & LOW PRESSURE BLADDER PULSATION DAMPERS (standard units)		Drg.No AV.AI.MP-BP.IN.DOC	Rev. 24	Date Sep-19 / Scale none

A26≡260bar
A18≡180bar
A12≡120bar
A11≡110bar
A10≡100bar

ORDER EXAMPLE: U007 A12 V 1 AI

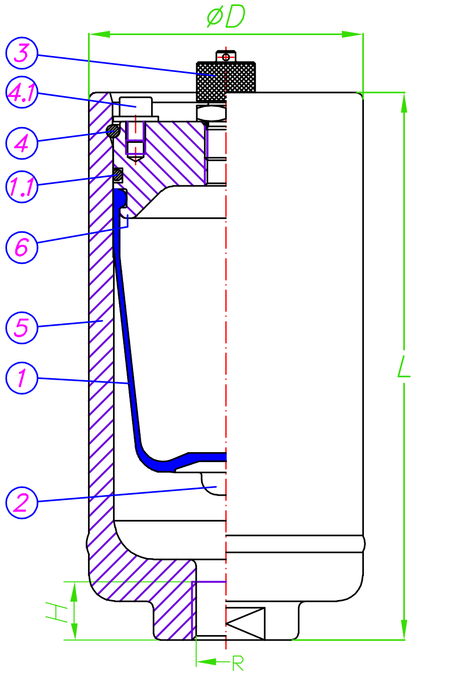
- Capacity: 0.65 litres
- A12≡120bar
- V= FKM Rubber Bladder
- 3/4" Standard Connection
- Body & insert material: AISI 316L

FOR HIGHER PRESSURES, SIZES, MATERIALS AND THREAD CONNECTIONS, PLEASE CONSULT

Value of "K": $\frac{\text{Maxi. Pressure}}{\text{Filling gas Pressure}} \leq$ K (@Constant Temp.)

Wall thickness acc. to AD-2000 code

Hydrostatic test pressure @1.5 * Design Pressure @ 20°C



H = MAXI. LENGTH OF THREAD CONNECTION

PULSATION DAMPER REF.	VOLUME (litres)	DESIGN PRESSURE (barg @50°C)	D (mm)	L (mm)	R (BSP)	H (mm)	WEIGHT (Kg)	K VALUE
U000	0.04	260	55	70	3/8"	14	0.8	2.5
U001	0.09			97			1.0	
U002	0.18	180	70	122	1/2"		1.8	
U003	0.36		85	168		16	3.6	3.0
U007	0.65	120	88	205	3/4"	20	3.8	3.5
U010	0.95	110	114	200		25	6.0	3.0
U015	1.50			245			6.8	3.5
U030	2.60		140	295	1"	27	10.5	
U040	3.80			386			12.2	5.0
U060	5.60	120	167	438	1-1/2"	35	24.0	
U100	10.40	100	217	442	2"		46.0	4.0
U150	15.00			625			52.5	5.0
U250	25.00		270	691	2-1/2"		70.0	4.0

No	DENOMINATION	QT.	MATERIALS
6	COVER	1	AISI 316L
5	BODY	1	AISI 316L
4.1	BOLT	2	ISO7380 A4-70
4	RETAINING RING	1	DIN17224 (AISI 316)
3	FILLING N2 VALVE	1	AISI 316L (1/4" BSP)
2	INSERT	1	AISI 316L
1.1	"O" RING	1	NBR, BUTYL, EPDM & FKM
1	BLADDER	1	NBR, BUTYL, EPDM & FKM

Standard Bladder Rubbers: N=NBR, B=BUTYL, E=EPDM, V=FKM (EPDM not available for U000)

(Other Rubbers: Neoprene, Hypalon, HNBR, etc.)	N	B	E	V
Rubbers Max. Working Temperatures (°C)	+80 −15	+100 −30	+130 −30	+200 −20

TOLERANCES: External dimensions: ± 3% Volume: ± 2.5% Weight: ± 5%

Working Temperatures versus Working Pressures **

For a temperature of 80°C correspond design pressure x 0.87
" " " " 100°C " " " x 0.82
" " " " 130°C " " " x 0.78
" " " " 200°C " " " x 0.68

THE MAX. WORKING TEMPERATURE CAN BE REDUCED DEPENDING ON THE LIQUID IN CONTACT

ATTENTION! ALWAYS MUST BE MOUNTED VERTICALITY (VALVE 3 ON TOP)

Those Pulsation Dampeners ought to be filled with gas at 80% of the working pressure. It shall be done at the working temperature.

NOTE: The precharge with gas or air must be done slowly and with our charging tool Ref. BVXXXA1TM

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Customer	Customer Ref.	Replaced Drg.N°	Drawn	Approved
		AV.AI.MP.IN.DOC (Rev.20)	E.Ponsa	

Title	Drg.No	Rev.	Date	Scale
S.S.MEDIUM PRESSURE BLADDER PULSATION DAMPERS (standard units)	AV.AI.MP.IN.DOC	21	Set-19	none

FOR HIGHER PRESSURES,TEMPERATURES, SIZES, AND MATERIALS AND THREADED CONNECTIONS, PLEASE CONSULT

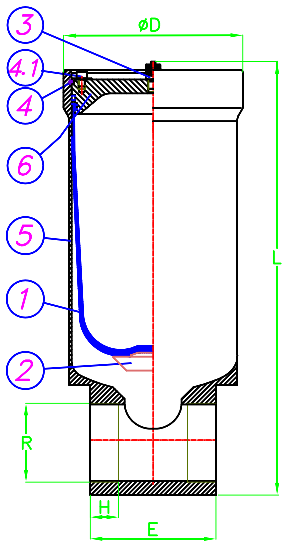
A02≡20bar
A03≡30bar
A04≡40bar
A05≡50bar

REFERENCE EXAMPLE : U030 A03 V 2 AI

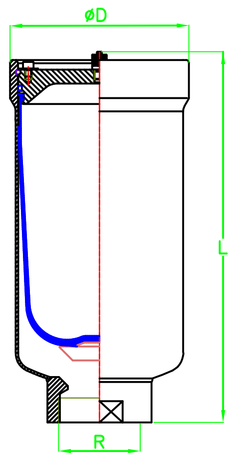
Capacity: 2.6 litres
A03≡30bar
V= FKM Rubber Bladder
2"Two Standard Connection ports
Body & insert material: AISI 316L

REFERENCE EXAMPLE : U030 A03 V 1 AI BB

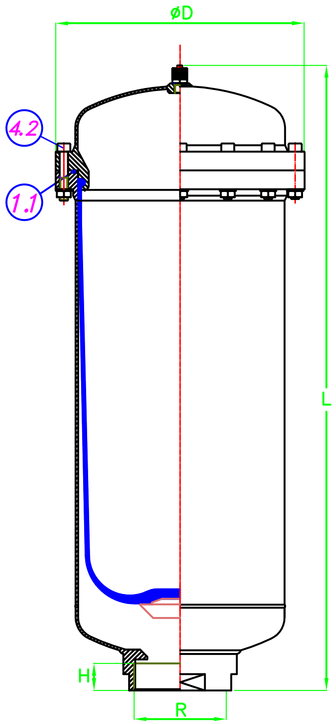
2"One Standard Connection ports
Big Bore connection port



IN LINE TWO CONNECTION PORTS



BIG BORE
U010 TO U250



BIG BORE (U350)

H = MAXI. LENGTH OF THREAD CONNECTION

Wall thickness acc. to AD-2000 code

Value of"K": $\frac{\text{Maxi. Pressure}}{\text{Filling gas Pressure}} \leq$ K (@Constant Temp.)

Hydrostatic test pressure @ 1.5 * Design pressure @ 20°C

PULSATION DAMPER Reference	VOLUME (litres)	DESIGN PRESSURE (bar-g @20°C)	D (mm)	E (mm)	L (mm) TWO PORTS	L (mm) BIG BORE	R (BSP)	H (mm)	WEIGHT (Kg) TWO PORTS	WEIGHT (Kg) BIG BORE	K VALUE
U007	0.65	50	88	66	231	na	1"	22	3.5	na	3.5
U010	0.95	40	113	81	251	220	1-1/2"	24	6	4.4	3.0
*U015	1.50				298	267			4.5	4.6	3.5
U030	2.60	30	140	100	346	310	2"	26	11	6.4	
*U040	3.80				449	413			11.5	7.2	4.5
*U060	5.60	40	167	120	506	442	2-1/2"	33	19.5	12	
*U100	10.40	30	217	155	547	445	4"		38	18	4.0
*U150	15.00				757	655			42	22	4.5
*U250	25.00	20	270	212	780	754			63	31	4.0
*U350	35.00		302		860	766					2.5

No	DENOMINATION	QT.	MATERIALS
6	COVER	1	AISI 316L
5	BODY	1	AISI 316L
4.2	BOLTS & NUTS M10	20	DIN 912 & 934 A4-70
4.1	BOLTS	3	DIN 912 & 934 A4-70
4	RETAINING RING	1	DIN17224 (AISI 316)
3	INFLATING N_2 VALVE	1	AISI 316L (1/4" BSP)
2	INSERT	1	PVDF △
1.1	"O" RING	1	NBR, BUTYL, EPDM & FKM
1	BLADDER	1	NBR, BUTYL, EPDM & FKM

Standard Bladder Rubbers: N=NBR, B=BUTYL, E=EPDM, V=FKM

(Other Rubbers: Neoprene, Hypalon, HNBR, etc.)	N	B	E	V
Rubbers Max. Working Temperatures (°C)	+80 -15	+100 -25	+130 -25	+135 △ -25

TOLERANCES:
External dimentions: ± 2mm
Volume:±2.5% Weight:± 5%

Working Temperatures versus Working Pressures **

For a temperature of 80°C correspond design pressure x 0.87
" " " " 100°C " " " x 0.82
" " " " 135°C " " " x 0.76

THE MAX. WORKING TEMPERATURE CAN BE REDUCED DEPENDING ON THE LIQUID IN CONTACT

*ATTENTION! ALWAYS MUST BE MOUNTED VERTICALITY(VALVE 3 ON TOP)

Those Pulsation Dampeners ought to be filled with gas at a value of 0.80x the pressure to stabilize and that at the working temperature

NOTE: The precharge with gas or air must be done slowly and with our charging tool Ref. BV(***)A1TM

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Customer	Customer Ref.	Replaced Drg.N°	Drawn	Approved
			K.Ventura	M.Carcaré

Title	Drg.No	Rev.	Date	Scale
SPECIAL S.S.MEDIUM AND LOW PRESSURE "IN LINE" & BIG BORE, BLADDER PULSATION DAMPERS	AV.AI.MP-BP.DP.BB.IN.DOC	05	July21	none

A03≡30bar	
A04≡40bar	
A05≡50bar	
A06≡60bar	
A09≡90bar	

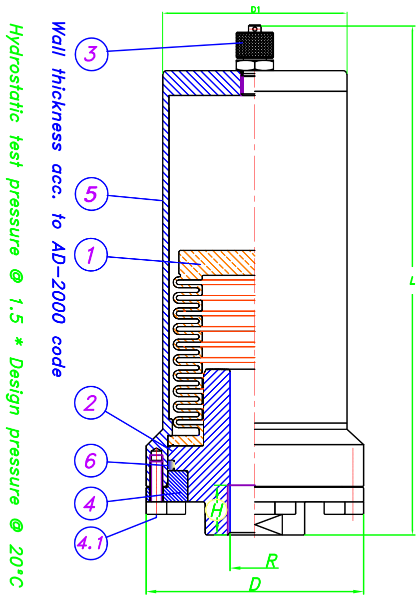
ORDER EXAMPLE: F030 A04 T 1 AI
- Capacity: 2.6 litres
- A04≡40bar
- T= PTFE Bellows
- 1" Standard Connection
- Body & nozzle material: AISI 316L

MAX. WORKING PRESSURE / FILLING GAS PRESSURE < K

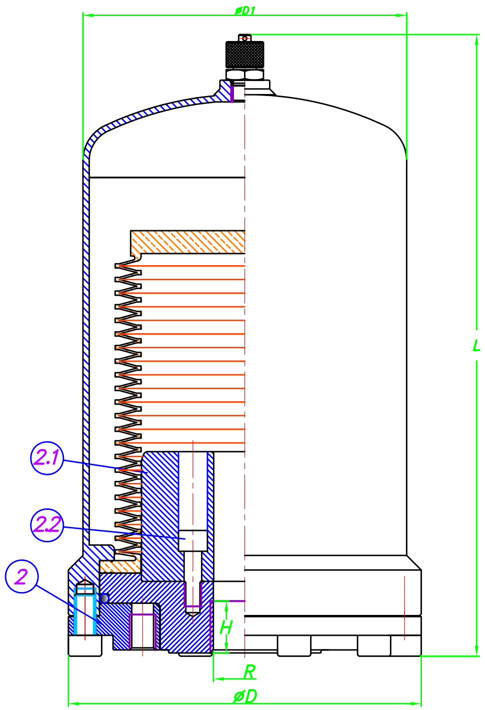
PULSATION DAMPER MODEL	MAXI. δV ADMITED (c.c.)**	VOLUME (litres)	DESIGN PRESSURE (bar-g)	D (mm)	D1 (mm)	L (mm)	R (BSP)	H (mm)	WEIGHT (Kg.)	K VALUE
F002	12	0.15	90	71	60	178	1/2"	16	1.4	1.2
F003	20	0.30	50	84	64	234			2.2	
F007	80	0.70	60	105	89	250	3/4"	25	4.1	
F015	450	1.50	50	130	114	254			6.6	1.6
F030	950	2.60	40	170	156	295	1"	27	10.6	1.8
F040	1000	3.80				350			11.0	1.6
F060	850	5.60				475			12.3	1.3
F100	2400	10.00	30	250	206	441	2"	35	24.0	1.5
F150	2900	15.00				610			26.0	1.4

Nº	DENOMINATION	QT.	MATERIALS
6	SEAL GASKET	1	SILICONE
5	BODY	1	AISI 316L
4.1	BOLTS	7 to 10	DIN 912 A4-70
4	RETAINING NUT	1	AISI 316L
3	FILLING N_2 VALVE	1	AISI 316L (1/4" BSP)
2.2	BOLTS	3	DIN 912 A4-70
2.1	GUIDING NOZZLE	1	PTFE
2	NOZZLE	1	AISI 316L
1	BELLOWS	1	PTFE

ATTENTION! ALWAYS MUST BE MOUNTED VERTICALITY (VALVE 3 ON TOP)



F002 to F015



F030 to F150

H = MAXI. LENGTH OF THREAD CONNECTION

Working Temperatures versus Working Pressures

For a temperature of 100°C correspond design pressure x 0.82
" " " " 150°C " " " x 0.75
" " " " 200°C " " " x 0.68

WORKING LIMITS TEMPERATURES(°C): -40° / +200°C

Those Pulsation Dampeners ought to be filled with gas at 90% of the working pressure. It shall be done at the working temperature.

TOLERANCES: External dimentions: ± 3% Volume: ±2.5% Weight: ±5%

** $\Delta V \geq C/2$ for a single head pump ("C"=Head pump volume)
$\Delta V \geq C/5$ for a duplex heads pump
$\Delta V \geq C/12$ for a three heads pump

NOTE: The precharge with gas or air must be done slowly and with our charging tool Ref. BVXXXA1TM

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Customer	Customer Ref.	Replaced Drg.Nº	Drawn	Approved
		AFT.AI.BP.IN.DOC (Rev.23)	E.Cortina	M.Carcaré

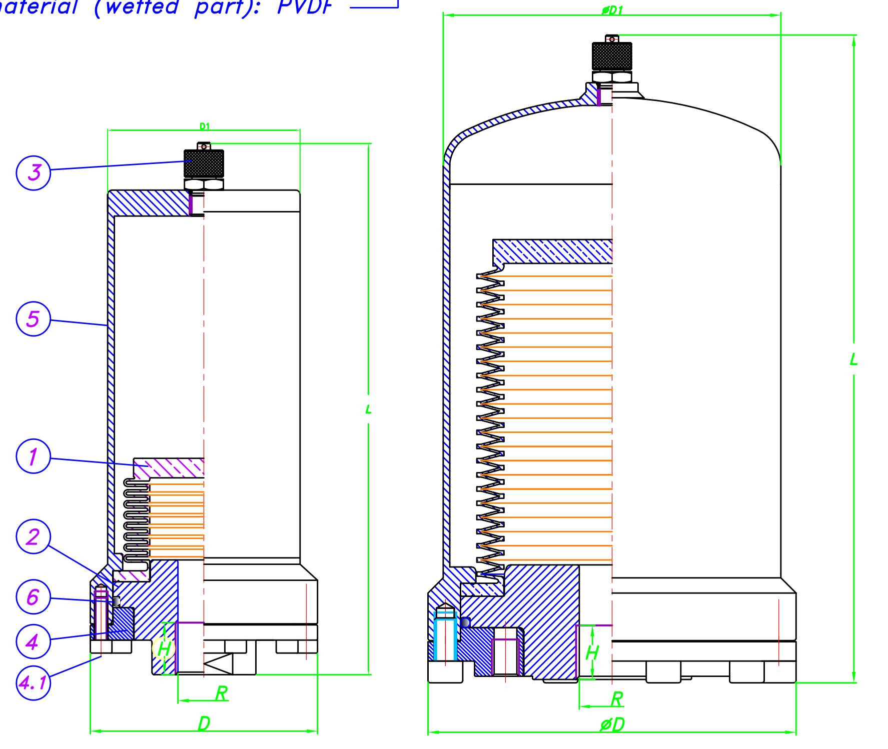
Title	Drg.No	Rev.	Date	Scale
PTFE BELLOWS PULSATION DAMPER, SS BODY & NOZZLE (Wet parts in PTFE and Stainless Steel)	AFT.AI.BP.IN.DOC	24	Apr-22	-

ORDER EXAMPLE: F030 A02 T 1 AI/PD

Capacity: 2.6 litres
A02≡20bar
T= PTFE Bellows
1" Standard Connection
Body & nozzle material: AISI 316L
Nozzle material (wetted part): PVDF

$\frac{\text{MAX. WORKING PRESSURE}}{\text{FILLING GAS PRESSURE}} < K$

Wall thickness acc. to AD-2000 code
All parts in contact with fluid made in PVDF, PTFE, PVC or PE
Hydrostatic test pressure @ 1.5 * Design pressure @ 20°C



F002 to F015 F030 to F150

H = MAXI. LENHTH OF THREAD CONNECTION

PULSATION DAMPER MODEL	MAXI. δV ADMITED (c.c.) **	VOLUME (litres)	D (mm)	D 1 (mm)	L (mm)	R (BSP)	H (mm)	WEIGHT (Kg.)	K VALUE
F002	12	0.15	71	60	178	1/2"	16	1.4	1.2
F003	20	0.30	84	64	234			2.2	
F007	80	0.70	105	89	250	3/4"	25	4.1	
F015	450	1.50	130	114	254			5.6	1.6
F030	950	2.60	170	156	295	1"	27	10.6	1.8
F040	1000	3.80			350			11.0	1.6
F060	850	5.60			475			12.3	1.3
F100	2400	10.00	250	206	441	2"	35	24.0	1.5
F150	2900	15.00			610			26.0	1.4

Nº	DENOMINATION	QT.	MATERIALS
6	SEAL GASKET	1	SILICONE
5	BODY	1	AISI 316L
4.1	BOLTS	7 to 10	DIN 912 A4-70
4	RETAINING NUT	1	AISI 316L
3	FILLING N_2 VALVE	1	AISI 316L (1/4" BSP)
2	NOZZLE	1	(+) PTFE, PE, PVC, PVDF
1	BELLOWS	1	PTFE

ATTENTION! ALWAYS MUST BE MOUNTED VERTICALITY (VALVE 3 ON TOP)

** $\Delta V \geq C/2$ for a single head pump
$\Delta V \geq C/5$ for a duplex heads pump
$\Delta V \geq C/12$ for a three heads pump

NOTE: The precharge with gas or air must be done slowly and with our charging gas Ref. BVXXXAITM

Working Temperatures versus Working Pressures

For a temperature of 100°C correspond design pressure x 0.82
" " " " 150°C " " " x 0.75

WORKING LIMITS TEMPERATURES(°C):		
(0° / +60°C for PVC)	(+) Polyethylene= PE	MAX.WORKING
(-15° / +70°C for PVDF & PE)	(+) PVC = PC	PRESSURE: 20 bar-g
(-40° / 200°C for PTFE)	(+) PVDF = PD	
	(+) PTFE = TF	

THE MAXI TEMPERATURE CAN BE REDUCED DEPENDING ON THE LIQUID IN CONTACT

Those Pulsation Dampeners ought to be filled with gas at a value of 0.90x the pressure to stabilize and that at the working temperature

TOLERANCES:
External dimentions: 3%
Volume: ± Weight: ±5%

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Customer	Customer Ref.	Replaced Drg.Nº	Drawn	Approved
		AFT.AI.BP.IN.PL.DOC (Rev.24)	E.Cortina	M.Carcaré
Title	PTFE BELLOWS PULSATION DAMPER, SS BODY & PLASTIC NOZZLE (Wet parts in PTFE and plastic)	**Drg.No**	**Rev.**	**Date** / **Scale**
		AFT.AI.BP.IN.PL.DOC	25	Nov-23 / -

ORDER EXAMPLE. F030 A03 I 1 AI

Capacity: 2.4 litres

A03=30bar

AISI 316Ti Bellows

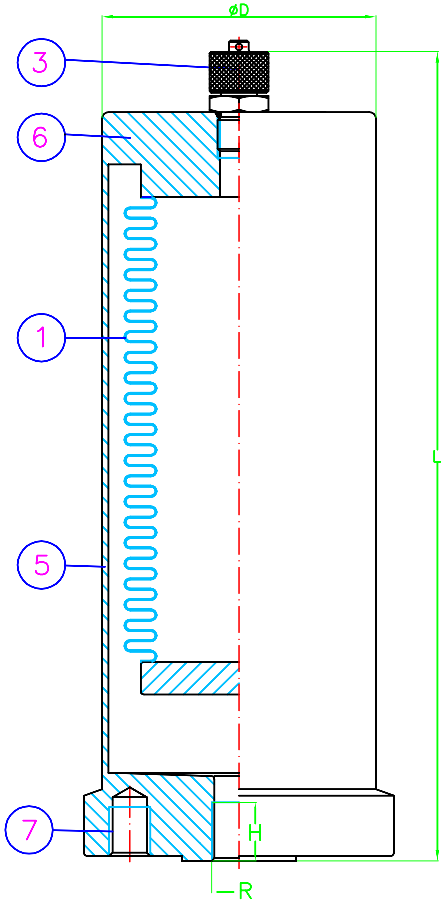
1" Standard Connection

Body material: AISI 316L

Wall thickness acc. to AD-2000 code

ASME "U" certificate 56.636. Consult for MAWP according SEC. VIII, DIV.1

Hydrostatic test pressure @ 1.5 * Design pressure @ 20°C



H = MAXI. LENGTH OF THREAD CONNECTION

PULSATION DAMPER MODEL	MAXI. dV ADMITED (c.c.) **	VOLUME (litres)	DESIGN PRESSURE (bar-g)	D (mm)	L (mm)	R (BSP)	FLANGE DN	H (mm)	WEIGHT (Kg)
F007	168	0.70	50	70	178	1/2"	1/2"	16	1.4
F015	418	1.45	40	88	250	3/4"	3/4"	25	4.1
F030	800	2.40	30	104	254	1"	1"	27	6.6
F040	1200	3.70			295				10.6
F060	1850	6.00	40	156	350	1-1/2"	1-1/2"	35	11.0
F100	3500	10.20	30	206	441	2"	2"		12.3
F150	4400	15.00			475				24.0

Precharge pressure ≤ 16 bar-g @ 20°C (*)

(*) Precharge pressure limited by the separator element (bellows).

For higher pressures and for (***) variable working pressures and/or temperatures, HIDRACAR has special designs. Please consult.

Nº	DENOMINATION	QT.	MATERIALS
7	INTEGRATED FLANGE (OPTIONAL)	1	ANSI B16.5 #300
6	GAS COVER	1	AISI 316L
5	BODY	1	AISI 316L
3	FILLING N_2 VALVE	1	AISI 316L (1/4" BSP)
1	BELLOWS	1	AISI 316 Ti

ATTENTION! ALWAYS MUST BE MOUNTED VERTICALITY (VALVE 3 ON TOP)

** ΔV≥C/2 for a single head pump ("C"=Head pump volume)

ΔV≥C/5 for a duplex heads pump

ΔV≥C/12 for a three heads pump

NOTE: The precharge with gas or air must be done slowly and with our charging tool Ref. BVXXXA1TM

For a temperature of 100°C correspond design pressure x 0.82

" " " " 200°C " " " x 0.68

" " " " 300°C " " " x 0.59

WORKING LIMITS TEMPERATURES(°C): -50° / +300°C

Those Pulsation Dampeners ought to be filled with gas at 90% of the working pressure. It shall be done at the working temperature.

TOLERANCES:
External dimentions:± 3%
Volume: ±2.5% Weight:±5%

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Customer	Customer Ref.	Replaced Drg.Nº	Drawn	Approved
			E.Ponsa	M.Carcaré

Title	Drg.No	Rev.	Date	Scale
PULSATION DAMPER WITH SS BELLOWS & BODY	AFI.AI.BP.IN.DOC	3	Mar-21	-

ORDER EXAMPLE: M030 A03 D 1 AI

A02≡20bar
A03≡30bar
A04≡40bar
A05≡50bar
A10≡100bar
A20≡200bar

Capacity: 2,8 litres
A03≡30bar
D=TFM1705+FKM Double Membrane
1-1/2" Standard Connection
Body & insert material: AISI 316L

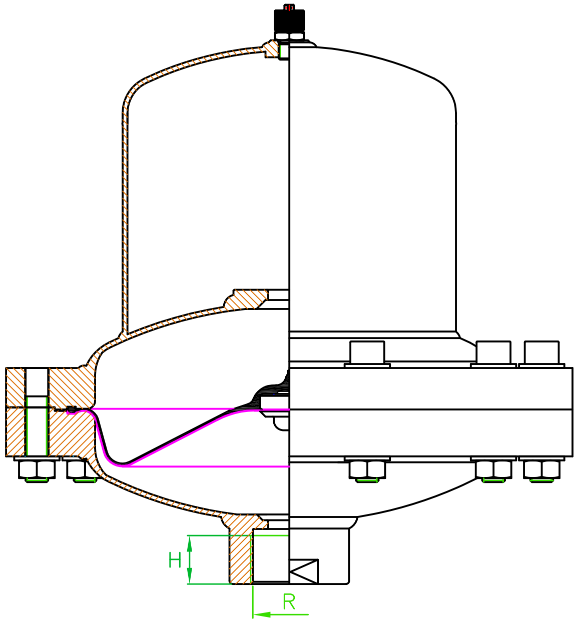
FOR HIGHER PRESSURES, SIZES, MATERIALS AND THREAD CONNECTIONS, PLEASE CONSULT

Value of "K": $\frac{\text{Maxi. Pressure}}{\text{Filling gas Pressure}} \leq 2$ (@Constant Temp.)

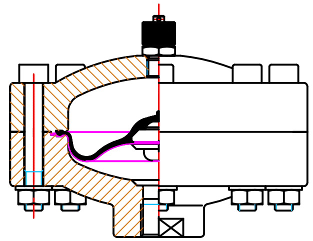
⊕ In these models the value of "K" ≤ 1.5 (@ Constant Temp.)

Wall thickness acc. to AD-2000 code

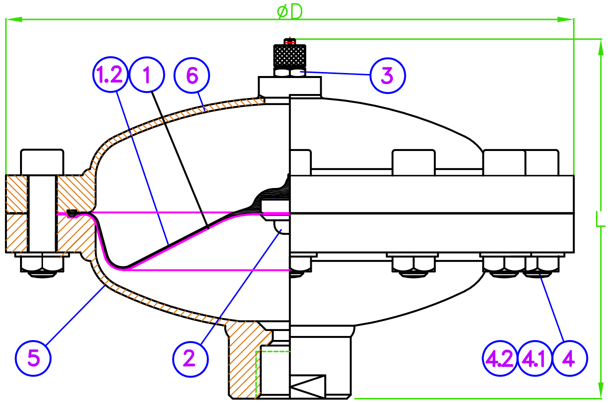
Hydrostatic test pressure @ 1.5 * Design pressure @ 20°C



M040 & M100



M001 to M004



M008 to M030 & M060

PULSATION DAMPER MODEL	VOLUME (litres)	DESIGN PRESSURE (bar-g)	D (mm)	L (mm)	R (BSP)	H (mm)	WEIGHT (Kg)
M001	0.08	150	100	96	3/8"	16	1.7
M002	0.2	200	140	100	1/2"	14	5.2
M004	0.4	100	164	122		16	9.2
M008	0.8	50	180	150	3/4"	20	4.7
M012	1.2	34	224	160			7.5
M030	2.8	25	289	180	1-1/2"	30	15.5
⊕M040	4.0			275			17.0
M060	5.6	20	340	233	2"		24.5
⊕M100	10.0			398			26.0

6	UPPER SHELL	1	AISI 316L
5	LOWER SHELL	1	AISI 316L
4.2	NUTS	8 to12	DIN 934 A4-70
4.1	WASHERS	8 to12	DIN 125 A4-70
4	BOLTS	8 to12	DIN 912 A4-70
3	FILLING N_2 VALVE	1	AISI 316L(1/4"BSP)
2	INSERT (button)	1	AISI 316L
1.2	MEMBRANE	1	FKM
1	MEMBRANE	1	PTFE (TFM1705)
Nº	DENOMINATION	QT.	MATERIALS

ATTENTION! ALWAYS MUST BE MOUNTED VERTICALITY (VALVE 3 ON TOP)

H = MAXI. LENGTH OF THREAD CONNECTION

TEMPERATURES RANGE
-20° to +200°C

Working Temperatures versus Working Pressures

For a temperature of 100°C correspond design pressure x 0.82
" " " " 150°C " " " x 0.75
" " " " 200°C " " " x 0.68

TOLERANCES:
External dimentions:±3%
Volume:±2.5% Weight:±5%

Those Pulsation Dampeners ought to be filled with gas at 90% of the working pressure. It shall be done at the working temperature.

NOTE: The precharge with gas or air must be done slowly and with our charging tool Ref. BVXXXA1TM

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Customer	Customer Ref.	Replaced Drg.Nº	Drawn	Approved
		AM.AI.BP.IN.DOC (Rev.26)	P.Bascompta	M.Carcaré
Title: S.S.PULSATION DAMPER DOUBLE MEMBRANE		Drg.No: AM.AI.BP.IN.DOC.	Rev. 27	Date: Jan-24 / Scale: none

WORKING TEMPERATURES VERSUS WORKING PRESSURES
FOR A W.TEMPERATURE OF 90°C CORRESPOND THE M.W.PRESSURE x0,85

CHARGING WITH GAS (DRY N2) OR COMPRESSED PURIFIED AIR

TEST PRESSURE(@ 20°C)= DESIGN PRESSURE X1.5

MAXI. W.TEMPERATURE: 90°C IF CLOSED LIQUID 9 IS WATER AND GAS FILLING PRESSURE >2 BAR

** Depending on the circuit data, this size can be different

FOR HIGHER PRESSURES, TEMPERATURES AND OTHER CONNECTION PORTS PLEASE CONSULT *

IN LINE PULSATION TRANSMITTER REF. (23)	CONNECTION PORTS		Bladder Damp. DESIGN PRESSURE (Bar) @ 20°C *	D (mm)	L(mm)		A (mm)	B (mm)	C (mm)	E (mm)	F (mm)	WEIGHT(Kg)		BLADDER DAMPER REF. **
	DIN11864-1	ISO1127			DIN	ISO						FIG.I	FIG.II	
L001A05(#)2AI-DT-	DN15/DN25		50	84	286	293	240	85	127					U007
L002A06(#)2AI-DT-	DN32/DN40	DN25/DN32	40	101	352	343	332	112	127					U015
L004A07(#)2AI-DT-	DN50/DN65		30	149	442	421	532	170	127					U060

(E)= For EPDM rubber hose; (S)= For Silicone rubber hose

wall thickness calculation according to EN 14359 code & ASME ("U" STAMP AVAILABLE)

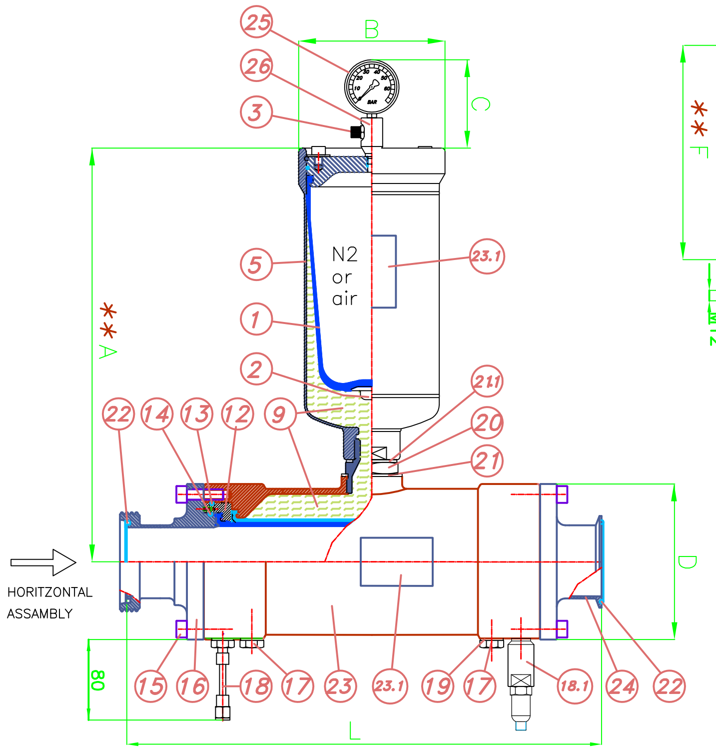

FIG. "I"

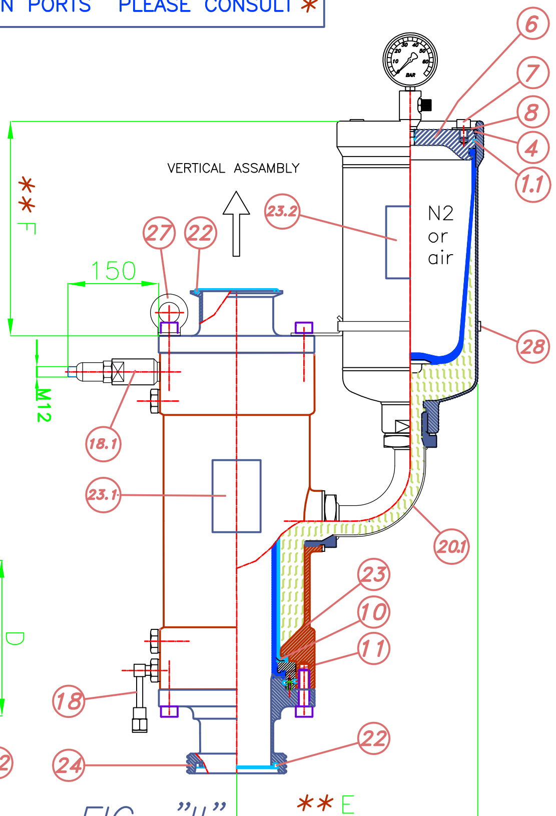

FIG. "II"

We reserve the right to change without notice

DIMENSION TOLERANCES: ±3mm

N°	DENOMINATION	QT.	MATERIALS
28	BLADDER DAMPENER SUPPORT	1	AISI 303
27	HANG EYEBOLT	1	AISI 303
26	"T" ADAPTOR	1	AISI 303
25	PRESSURE GAUGE	1	AISI 304
24	PORTS CONNECTION	2	DIN-11851
23.2	IDENTIFICATION LABEL	1	ADHESIVE PLASTIC
23.1	WELD NAMEPLATE	1	AISI 316L
23	IN LINE SHELL	1	AISI 316L
22	DIN-11851 or ISO-1127 Seal	2	EPDM or SILICONE (FDA)
21.1	SEAL WASHER	1	AISI 316L
21	SEAL WASHER	1	AISI 316L
20.1	BENDED TUB ADAPTOR	1	AISI 316L
20	ADAPTOR	1	AISI 316L
19	SEAL WASHER	4	AISI 316L
18.1	PLUG 1/4" BSP PORT CONNECTION	1	AISI316 FOR ELECTRONIC SENSOR
18	WINDOWS TUBE	1	FOR VISUAL HOSE RUPTURE
17	FILLING PLUG 1/4"BSP	2	AISI 316L
16	FLANGE CONNECTIONS	2	AISI 316L
15	RETAINING BOLTS	16	AISI 316L
14	O- RING	2	EPDM or SILICONE (FDA)
13	O- RING	2	EPDM or SILICONE (FDA)
12	SUPPORTING RING	2	AISI 316L
11	INTERNAL RUBBER HOSE	1	EPDM or SILICONE (FDA)
10	EXTERNAL RUBBER HOSE	1	EPDM or SILICONE (FDA)
9	SILICONE OIL (FDA) OR DESTILATED WATER		
8	WASHER	1	AISI 316L
7	BOLT	1	AISI 316L
6	COVER	1	AISI 316L
5	BODY TOP BLADDER DAMPENER	1	AISI 316L
4	RETAINING RING	1	AISI 316
3	CHARGING GAS VALVE	1	AISI 316L (1/4"BSP or Vg8)
2	INSERT	1	AISI 316L
1.1	O- RING	1	EPDM
1	DAMPENER BLADDER	1	EPDM or SILICONE (FDA)

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Aplication:	FOOD, BEVERAGE & PHARMACEUTICAL CIRCUITS	Drawn	Approved
		K. Ventura	M.Carcaré
Title	S.S.LOW PRESSURE PULSATION DAMPERS WITH IN LINE RUBBER HOSES	Rev.09.07.2021	Date / Scale
		14	02.12.19 / —

FOR HIGHER PRESSURES, TEMPERATURES AND OTHERS PORTS CONNECTIONS PLEASE CONSULT
ALSO AVAILABLE IN AISI 316L CONSTRUCTION

Nº	DENOMINATION	QT.	MATERIALS
23	IN LINE BODY	1	POLYPROPYLENE
18	PLASTIC WINDOWS TUBE	1	FOR VISUAL HOSE RUPTURE
17	FILLING PLUG 1/4"BSP	2	AISI 316L
16	FLANGE CONNECTIONS	2	PVC, POLIPROPYLENE, PVDF
15	RETAINING BOLTS	16	AISI 316L
14	O– RING	2	EPDM, FKM, NBR, SILICONE
13	O– RING	2	EPDM, FKM, NBR, SILICONE
12	SUPORTING RING	2	POLIPROPILENE
11	INTERNAL RUBBER HOSE	1	EPDM, FKM, NBR, SILICONE

IN LINE SHELL REFERENCE	MAX. PRESSURE DESIGN **	D (mm)	L (mm) *	V_0 (c.c.)	R (BSP)
L002A01(#)2PL–ST–DN20	10	120	319.5	745	3/4"
L002A01(#)2PL–ST–DN25					1"
L002A01(#)2PL–ST–DN32					1.1/2"
L004A01(#)2PL–ST–DN40		160	440.5	1700	2"
L004A01(#)2PL–ST–DN50					2.1/2"
L004A01(#)2PL–ST–DN65					3"

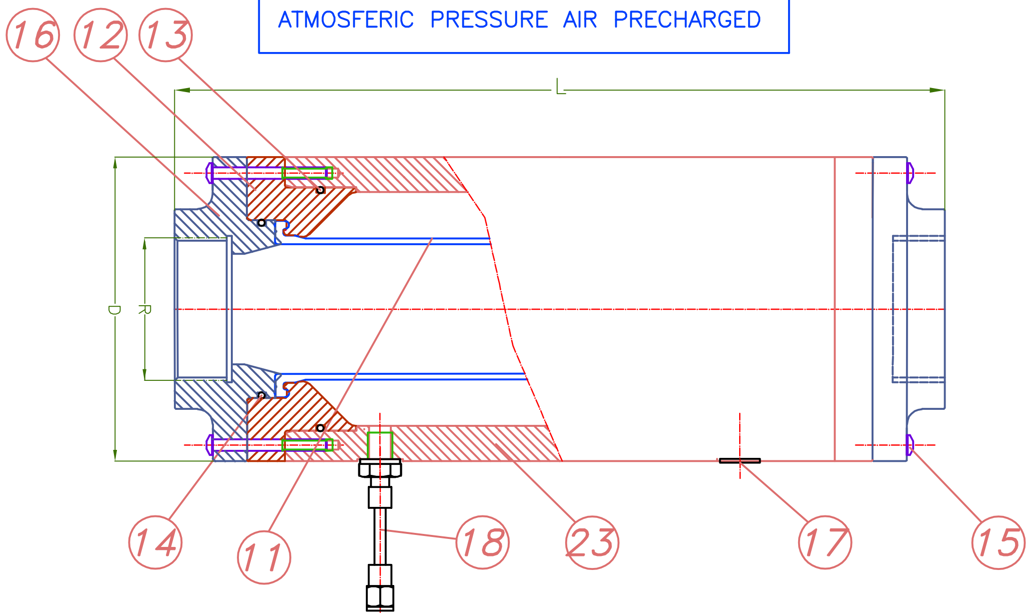
MAXI. WORKING TEMPERATURE: 60°C

** MAXI. WORKING PRESSURE: 4 BARG

ATMOSFERIC PRESSURE AIR PRECHARGED

(E)= For EPDM rubber HOSE; (S)= For Silicone; (V)= FKM; (N)=NBR

* This dimention can be variable according the connection type



DIMENTIONS TOLERANCES: ±3%

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Aplication: MAINLY SUCTION PUMPS LINES		Drawn: M.Carcaré	Approved: M.Carcaré
Title: PLASTIC LOW PRESSURE PULSATION DAMPER WITH IN LINE RUBBER HOSE		Rev.	Date: 13.01.20 / Scale: —

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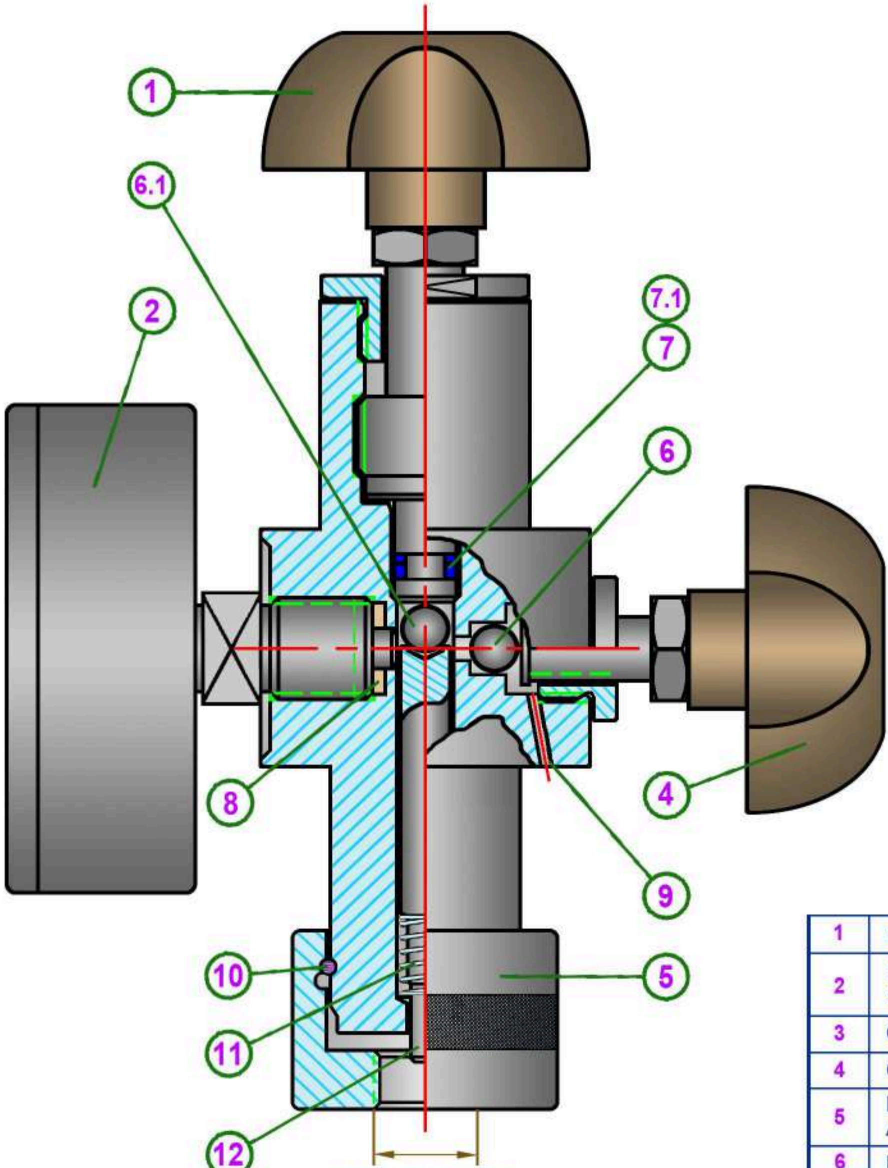
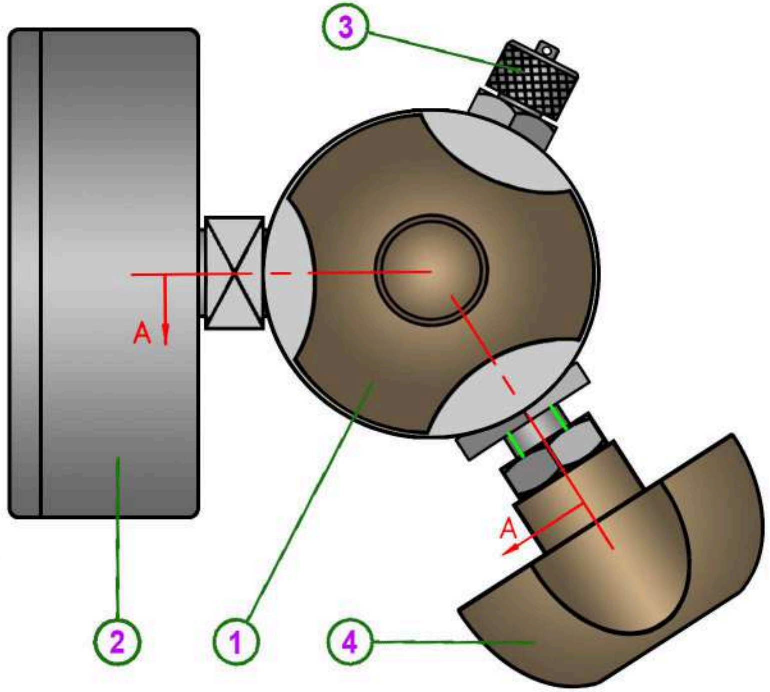


Height 140mm

Section A - A



NOTE: The scale range of the pressure gauge should be approx. 30% higher than the value of the gas pre-charge.

PRESSURE GAUGE SCALE RANGE	GAS BLOCK REFERENCE CODE
6 bar	BV006A1TM
16 bar	BV016A1TM
25 bar	BV025A1TM
40 bar	BV040A1TM
60 bar	BV060A1TM
160 bar	BV160A1TM
250 bar	BV250A1TM
400 bar	BV400A1TM
600 bar	BV600A1TM
1,000 bar	BV1000A1TM

Body & nuts material:
1.0718 steel with electroless nickel plating.

1	DAMPENER / ACCUMULATOR CHARGING VALVE CORE DRIVER HANDLE		
2	PRESSURE GAUGE (WITH SCALE RANGE ACCORDING TO MAXIMUM CHARGING PRESSURE)		
3	GAS SUPPLY HOSE ATTACHMENT CONNECTION VALVE		
4	GAS PURGE RELEASE HANDLE		
5	DAMPENER / ACCUMULATOR GAS CHARGING VALVE KNURLED ATTACHMENT RING NUT		
6	PURGE SHUTTER VALVE BALL	6.1	TRANSFER BALL
7	O-RING (ref.: HC2008-N)	7.1	BACK UP RING (ref.: HC8008-N)
8	PRESSURE GAUGE SEAL	9	PURGE GAS EXHAUST HOLE
10	ATTACHMENT RING NUT RETAINING RING		
11	SPRING	12	VALVE CORE DEPRESSOR PIN

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Customer	Customer ref.	Replaces drawing	Drawn by	Approved by
		BV(***)A1TM (Rev. 06)	E.Ponsa	M. Carcaré

Title: CHARGING AND CONTROL GAS BLOCK FOR OUR PULSATION DAMPENERS AND ACCUMULATORS

Drawing	Rev.	Date	Scale
BV(***)A1TM	07	26/04/17	1/1

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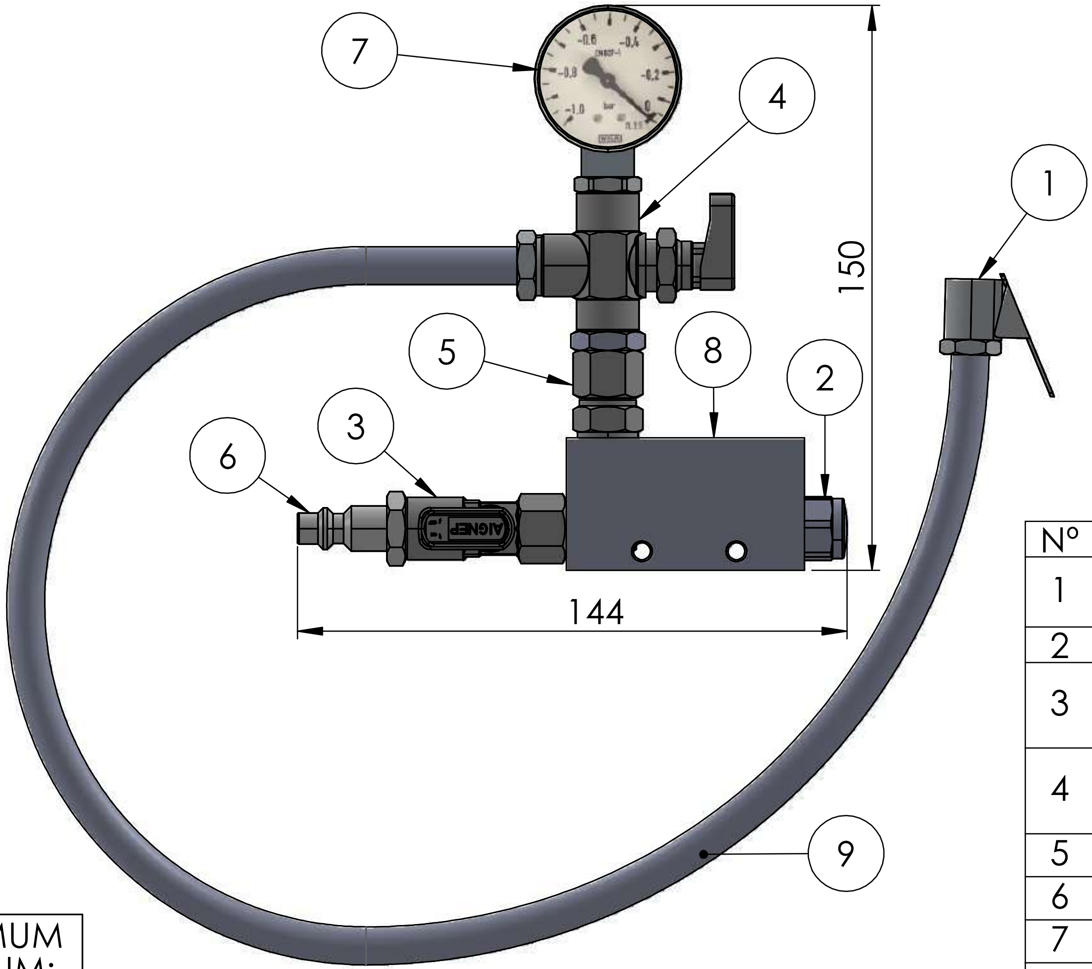
DATA SHEET	REFERENCE:	REV:
VACUUM KIT	BV-VAC	00

DESCRIPTION: VACUUM KIT FOR OUR PULSATION DAMPERS EQUIPPED WITH THE VG8 [004-AI-BP] VALVE OR ADACNEU [adacneu.5]. THIS DEVICE ALLOWS YOU TO CREATE A VACUUM INSIDE THE PULSATION DAMPERS AND THUS BE ABLE TO WORK AT PRESSURES BELOW ATMOSPHERIC.
NOTE: IF YOUR DEVICE DOES NOT HAVE A VG8 VALVE, WE CAN SUPPLY IT.



MAXIMUM PRESSURE:	MAXIMUM VACUUM:
6 bar-g	-0.85 bar-g

Nº	ITEM	MATERIAL
1	VG8 quick connector	Brass
2	Sound filter	Brass
3	Flow air control valve	Nickel plated brass/plastic
4	Check control valve	Nickel plated brass/plastic
5	Swivel fitting	Nickel plated brass
6	ISO 6150 adaptor	Nickel plated brass
7	Vacuum gauge	Brass/plastic
8	Venturi vacuum ejector	Aluminium
9	Tube 8 x 500 mm	Polyurethane

HIDRACAR S.A.

GAS CHARGING VALVE THREAD ADAPTOR

ADAPTADOR DE ROSCA PARA VÁLVULA DE CARGA DE GAS

ADACNEU.5

Adapts the thread of 1/4" BSP standard charging valves to the thread of the Vg8 valves so a tyre inflating kit can be used for charging with compressed air.

Adapta la rosca de las válvulas de carga estándar BSP de 1/4" a las de las válvulas Vg8 para poder cargar con aire comprimido, mediante la utilización de un kit de hinchado de neumáticos.

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HIDRACAR S.A.

STAINLESS STEEL "T" ADAPTER WITH PRESSURE GAUGE

ADAPTADOR EN "T" CON MANÓMETRO EN ACERO INOXIDABLE

BT#A-AI

Pressure gauge casing and "T" adapter made of stainless steel.
Carcasa del manómetro y adaptador en "T" de acero inoxidable.

600 bar adapter design pressure.
Presión de diseño del adaptador de 600 bar.

Pressure gauges available for pressures (#) of: 6, 10, 16, 25, 40, 60, 100, 120, 250, 300, 400 and 600 bar.

Manómetros disponibles para presiones (#) de: 6, 10, 16, 25, 40, 60, 100, 120, 250, 300, 400 600 bar.

Brass pressure gauge connection.
Conexión del manómetro de latón.

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HIDRACAR S.A.

SISTEMA DE SEGURIDAD ANTI-EXPLOSIÓN (*) POR INCENDIO MEDIANTE FUSIBLE DE TEMPERATURA

FIRE OVERPRESSURE EXPLOSION RISK PREVENTION (*) TEMPERATURE FUSE SAFETY SYSTEM

FST-AI/PD

(*) Our pulsation dampeners are designed with a minimum safety coefficient of 4:1.

(*) Nuestros amortiguadores de pulsaciones están diseñados con un coeficiente de seguridad mínimo de 4:1.

Releases the gas inside the accumulator when the surrounding temperature reaches160 ºC; and this way relieves the internal pressure and prevents the risk of explosion.

The same fuse is suitable for pressures between 10 bar and 1,000 bar.

Permite que el gas del interior del acumulador escape al exterior cuando la temperatura ambiente alcanza los 160 ºC; y así alivia la presión interior y evita una potencial explosión.

El mismo fusible sirve para presiones desde 10 ba hasta 1,000 bar.

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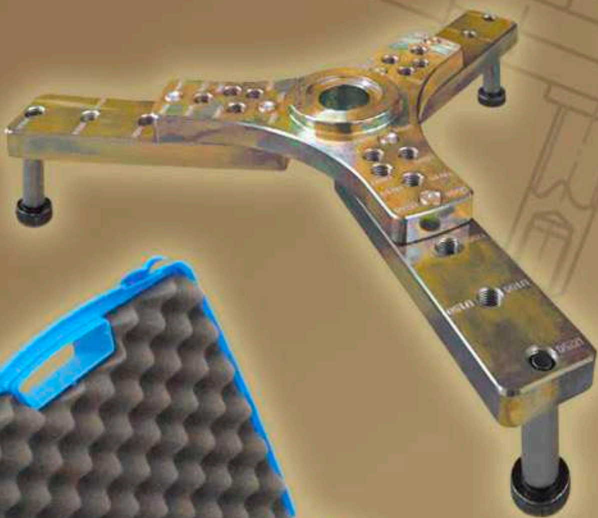
HIDRACAR S.A.

TOOL FOR A QUICK EXTRACTION OF THE BLADDER FROM ACCUMULATORS

DRB.A/B



HERRAMIENTA DE EXTRACCIÓN RÁPIDA DE LA VEJIGA DE LOS ACUMULADORES

Suitable for the whole range of our bladder type accumulators, except for U350.

Para toda la gama de nuestros acumuladores de vejiga, excepto el U350.

Enables bladder extraction without being necessary to disconnect the accumulator from the circuit.

Permite extraer la vejiga sin necesidad de desmontar el acumulador del circuito.

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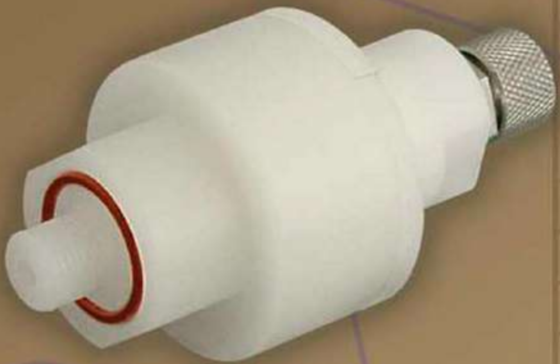
HIDRACAR S.A.

ANTI-CORROSION VALVE

Prevents that, when a corrosive liquid is circulating through the circuit, and in case the separator element (bladder, membrane or bellows) of the dampener gets broken, the corrosive liquid could corrode the stainless steel gas charging valve and escape to the exterior.

This anti-corrosion valve is supplied together with the standard gas charging valve.



004-AI + PVDF

VÁLVULA ANTI-CORROSIÓN

Evita que, cuando por el circuito circula un líquido corrosivo, y en caso de rotura del elemento separador (vejiga, membrana o fuelle) del amortiguador, el líquido pueda corroer la válvula de carga de gas de acero inoxidable y fugar al exterior.

Esta válvula anti-corrosión se suministra conjuntamente con la válvula de carga de gas estándar.

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HIDRACAR S.A.

ACCESSORY FOR CHARGING, PURGING AND VERIFYING THE PRESSURE OF OUR PULSATION DAMPENERS

ACCESORIO DE CARGA, PURGADO Y VERIFICACIÓN DE LA PRESIÓN DE NUESTROS AMORTIGUADORES DE PULSACIONES

ADAPTADOR "S" (W21.8x1/14" HEMBRA) "S" ADAPTER (W21.8x1/14" FEMALE)	ADAPTADOR "T" (W24.3x1/14" HEMBRA) "T" ADAPTER (W24.3x1/14" FEMALE)	ADAPTADOR "Y" (5/8" ISO 228) "Y" ADAPTER	ADAPTADOR "Z" (W21.8x1/14" MACHO) "Z" ADAPTER (W21.8x1/14" MALE)
			

BV#A1TM

Supplied with optional pressure gauges and connection hose adapter (S, T, Y or Z); as well as a connection hose for either low and medium pressures or for high pressures (600 and 1,000 bar) as required.

Se suministra con manómetros y adaptador de conexión (S, T, Y o Z) opcionales; así como con manguera de conexión para presiones bajas y medias o para presiones altas (600 y 1.000 bar) según el rango de presiones que se precise.

Range of available pressures (#):
10, 16, 25, 40, 60, 100, 160, 250, 300, 400, 600 and 1,000 bar.

Rango de presiones (#) disponibles:
10, 16, 25, 40, 60, 100, 160, 250, 300, 400, 600 y 1.000 bar.

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